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# MANAGING RUNOFF WATER QUALITY FROM CLAY SETTLING AREAS USED FOR INTENSIVE AGRICULTURAL PRODUCTION

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# MANAGING RUNOFF WATER QUALITY FROM CLAY SETTLING AREAS USED FOR INTENSIVE AGRICULTURAL PRODUCTION

### FINAL REPORT

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#### PERSPECTIVE

According to the Department of Environmental Protection, Bureau of Mine Reclamation, there are more than 110,000 acres of active and inactive clay settling areas in Florida as a result of phosphate mining and upgrading of ore. Because of the physical properties of the clays, the reclaimed settling areas are unsuitable for urban or suburban development. However, the clays are high in fertility and have high moisture holding capacities so that the settling areas do have great potential for intensive agriculture. Reclamation for intensive agricultural production would result in higher land values (and greater tax revenues to the counties) than if the lands were reclaimed to pasture or wildlife habitat.

The Mined Lands Agricultural Research and Demonstration Project was funded, beginning in late 1985, to study the technical and economic feasibility of agricultural production on phosphatic clay settling areas. The research has included: (1) identification of various crops and cropping systems suitable for production on phosphatic clay in central Florida; (2) development of soil management techniques for coping with a clay soil in a rainy environment; (3) participation in studies to assess the extent of any radionuclide hazard from consuming foods produced on phosphatic clay; and (4) analysis of production costs and markets for various crops. A comprehensive report published in 1996 (The Mined Lands Agricultural Research and Demonstration Project: Summary of Experiments and Extension Recommendations, FIPR Publication No. 03-090-128) summarized the findings from nearly ten years of research.

In the course of the Mined Lands Agricultural Research and Demonstration Project it was learned that crop production on phosphatic clay and timely access to the fields for critical management actions such as pest control and harvesting could be enhanced by creating large gently-sloped (2% grade) planting beds to promote runoff of precipitation and thereby reduce soil water-logging and mud puddle formation. However, the slightly increased slopes of the planting beds and the greater frequency of soil disturbance associated with intensive farming, compared to using the land for pasture, could possibly result in greater runoff volumes and greater sediment loads in the runoff. The purpose of this project was to quantify the impacts of agricultural production on the quantity and quality of runoff water from agricultural fields on a clay settling area and to examine techniques for minimizing or eliminating possible negative impacts on water quality. The study compared runoff from plots with a continuous cover crop (bermudagrass) versus plots with a corn and wheat rotation. They also evaluated a stilling (wet detention or settling) pond and chemical flocculants for reducing the discharge of nutrients and sediment.

Steven G. Richardson, Ph.D. Reclamation Research Director

#### ABSTRACT

Clay settling areas from phosphate mining in central Florida contain fertile, highly productive agricultural soils. However, gently sloped (2% grade) beds intended to improve surface drainage, combined with increased soil disturbance associated with intensive crop production, could lead to greater runoff volumes and sediment loads.

The objective of this work was to examine surface water quality discharged from agriculturally utilized phosphatic clay settling areas. Two preliminary replicated small plot (1 m x 1.5 m) field trials were used to describe the characteristics of runoff from bare, bermudagrass-covered, or ryegrass-covered phosphatic clay at either 2% or 8% slope. Results from the first small plot experiment were used to calibrate the GLEAMS (Groundwater Loading Effects of Agricultural Management Systems) model with respect to sediment and runoff predictions. Water quality measurements included runoff and sediment amounts and N and P concentrations.

The calibrated GLEAMS model was successfully used to predict runoff and sediment loading observed in a second small plot experiment. The GLEAMS model also predicted N loading in runoff and sediment, but over-predicted P. Sensitivity analysis showed that the current GLEAMS model does not have appropriate mechanisms for addressing the high mineral-P concentration of phosphatic clays.

Sediment loading varied with slope, and bare phosphatic clay generated greater than nine times as much sediment as ryegrass-covered small plots at the 2% slope. The amounts of N and P found in the runoff were more than values reported in the literature for native prairies, but much less than values observed for agricultural soils receiving P fertilization. P was strongly correlated with sediment.

Large field plots (approximately 1.2 ha each) were established in bermudagrass or corn followed by wheat. Both fields were landformed into macrobeds with 2% slopes. Flumes and automated water sampling equipment were installed at the discharge end of each macrobed. A weather station was used to collect rainfall amount, temperature, and wind data pertaining to the field plots. The corn/wheat rotation field produced more runoff events than the bermudagrass field. While all measures of N were low, measures of sediment and P from the cornfield were 2 to more than 6 times the concentration found in runoff from the bermudagrass field.

PERSPECTIVE	iii
ABSTRACT	V
EXECUTIVE SUMMARY	1
	1
INTRODUCTION AND BACKGROUND	3
Statement of Source & Magnitude of Problem Review of Pertinent Literature and Related Work in Progress	
Effect of Agricultural Management Practices on Runoff Quality Model Application on Runoff and Water Quality Enumeration of the Runoff and Water Quality	5
Small Plot Experiment Methods	
Small Plot Experiment, Green Bay Site	6
Small Plot Experiment Findings	9
Small Plot Experiment, Green Bay Site	9
Modeling Runoff Data from Small Plot Experiment, Ft. Green Site	11
Large Field Macrobed Experiment Methods	19
Materials and Methods	19
Filtration	
Sediment Sediment Phosphorus and Sediment Nitrogen	
Soluble Reactive Phosphorus (SRP)	
Total Soluble Phosphorus (TSP)	
Total Phosphorus (TP)	
Nitrate (NO <sub>3</sub> -N)	21
Ammoniacal-N (NH4 <sup>+</sup> -N)	
Total Soluble Nitrogen (TKN)	
Total Nitrogen (TN)	
Mehlich-3 Extraction Use of Chemical Precipitation and Coagulation Techniques	
Use of Chemical Freephation and Coagulation Feelinques	

## TABLE OF CONTENTS

LARGE FIELD MACROBED EXPERIMENT FINDINGS	23
Agronomic Data	23
Sediment Accumulation in the Pond	
Water Quality	24
Modeling Runoff from Large Macrobeds	30
Bermudagrass Macrobed	30
Corn/Wheat Macrobed	
Pond	38
Chemical Treatment of Suspended Clay Solids in Mined-Lands	
Runoff Waters	40
Soil Particle Size and Distribution at the Experimental Site	
Objective	42
Materials and Methods	
Reclamation Growing Area	
Reclamation Overflow Pond	
CONCLUSIONS/RECOMMENDATIONS	47
REFERENCES	49

## **TABLES OF CONTENTS (CONT.)**

## APPENDIXES

A.	Pond Survey Data	A-1
	Layout and Construction Details for Macrobed Experiment	
	Chemical Treatment of Suspended Solids in Mined-Lands Runoff Waters -	
	Laboratory Data	.C-1

## **LIST OF FIGURES**

# Figure

1.	Analytical Pathway for Runoff Samples	7
2.	Initial and Calibrated GLEAMS Model Predictions with Observed	
	Bermudagrass Sediment Values, Green Bay Site, 1995	9
3.	Predicted Bare Phosphatic Clay Sediment Values Using the Calibrated	
	GLEAMS Model and Observed Values, Green Bay Site, 1995	10
4.	Predicted Sediment Values Using the Calibrated GLEAMS Model	
	Compared to Observed Values from Phosphatic Clay with Alfalfa,	
	Green Bay Site, 1995	11
5.	Predicted and Observed Sediment as a Function of Slope and Cover,	
	Ft. Green Site, 1996	12
6.	Predicted and Observed Runoff from Small Plots as a Function of	
	Slope and Cover, Ft. Green Site, 1996	13
7.	Predicted and Observed N in Sediment as a Function of Slope and	
	Cover, Ft. Green Site, 1996	14
8.	Predicted and Observed P in Sediment as a Function of Slope and	
	Cover, Ft. Green Site, 1996	14
9.	Predicted and Observed N in Runoff as a Function of Slope and Cover,	
	Ft. Green Site, 1996	15
10.	Predicted and Observed P in Runoff as a Function of Slope and Cover,	
	Ft. Green Site, 1996	16
11.	Sensitivity Analysis of GLEAMS Parameters for Prediction of N,	
	Ft. Green Site, 1996	17
12.	Sensitivity Analysis of GLEAMS Parameters for Prediction of P,	
	Ft. Green Site, 1996	
13.	Predicted and Observed Runoff from Macrobed Planted in Bermudagrass	31
14.	Predicted and Observed Sediment Concentration from Macrobed Planted	
	in Bermudagrass	32
15.	Predicted and Observed Phosphate – PO <sub>4</sub> from Macrobed Planted in	
	Bermudagrass	
16.	Phosphate Versus Sediment in the Runoff from All Experimental Plots	33
17.	Predicted and Observed Nitrate (NO <sub>3</sub> ) in the Runoff from the Macrobed	
	Planted in Bermudagrass	33
18.	Predicted and Observed Ammonium (NH <sub>4</sub> ) in the Runoff from the	
	Macrobed Planted in Bermudagrass	
19.	Predicted and Observed Runoff from Macrobed Planted with Corn/Wheat	36
20.	Predicted and Observed Sediment Concentrations from Macrobed	
	Planted in Corn/Wheat	37
21.	Predicted and Observed Phosphate (PO <sub>4</sub> ) Concentrations from Macrobed	
	Planted in Corn/Wheat	37
22.	Predicted and Observed Nitrate (NO <sub>3</sub> ) Concentrations in the Runoff	
	from the Macrobed Planted in Corn/Wheat	37

## LIST OF FIGURES (CONT.)

# Figure

## Page

23.	Predicted and Observed Ammonium (NH <sub>4</sub> ) Concentrations in the	
	Runoff from the Macrobed Planted in Corn/Wheat	.38
24.	Measured Runoff from Both Macrobeds and Inflow and Outflow	
	of the Pond	.39
25.	Turbidity Levels After Chemical Treatment	.41
26.	a. Mean Particle Size, b. Silt (2-64 µm) Content, c. Clay (0-2 µm) Content,	
	and d. Sand (> 64 µm) Content of Sediments in the Reclamation Growing	
	Area	.44
27.	a. Mean Particle Size, b. Silt (2-64 µm) Content, c. Clay (0-2 µm) Content,	
	and d. Sand (> 64 µm) Content of Sediments in the Overflow Pond	.45

#### **EXECUTIVE SUMMARY**

The objective of this work, *Managing Runoff Water Quality from Clay Settling Areas Used for Intensive Agricultural Production*, was to enhance surface water quality discharged from agriculturally utilized phosphatic clay settling pond areas. Two preliminary replicated field trials using 1 m x 1.5 m plots were used to describe the characteristics of runoff from bare, bermudagrass, or ryegrass-covered phosphatic clay at either 2% or 8% slope. Results from the first small plot experiment (Green Bay Mine site) were used to calibrate the GLEAMS (Groundwater Loading Effects of Agricultural Management Systems) model with respect to sediment and runoff predictions. The calibrated model was then used to predict runoff and sediment from the second small plot experiment, which was conducted at the Ft. Green Mine site.

Water quality measurements included runoff and sediment amounts at both sites. Nitrate-N, ammonium-N, total Kjeldahl N, total P and Soluble Reactive P were measured and modeled only for the second small plot experiment.

The replicated small-plot research found that sediment loading varied with slope, and that bare phosphatic clay generated greater than nine times as much sediment as ryegrass-covered small plots at the 2% slope. The amounts of N and P found in the runoff were more than values reported in the literature for native prairies, but much less than values observed for agricultural soils receiving P fertilization. Therefore, phosphatic clay does pose a problem with respect to runoff water quality, but no more so than other agricultural lands.

The calibrated GLEAMS model was successfully used to predict runoff and sediment loading observed in the second small plot experiment. The GLEAMS model also predicted N loading in runoff and sediment, but over-predicted P. Sensitivity analysis showed that the current GLEAMS model does not have appropriate mechanisms for addressing the high mineral-P concentration of phosphatic clays. P was strongly correlated with sediment.

Large field plots were established in bermudagrass or temperate corn (approximately 1.2 ha each). Both fields were landformed into macrobeds with 2% slopes. Flumes and automated water sampling equipment were installed at the discharge end of each macrobed. A weather station was used to collect rainfall amount, temperature, and wind data pertaining to the field plots.

A pond was constructed to collect runoff water from both field plots. Automated sampling equipment was installed at both the inflow and outflow ends of the pond to record/sample water for water quality analysis. Additionally, 20 metal posts were placed throughout the pond in a grid fashion to note temporal changes in plant species within the pond. Changes in sediment levels throughout the pond were also noted using the measuring scales attached to each metal post.

During the second year of the project, the two agricultural fields produced five runoff events that could be sampled. The bermudagrass field had only three runoff events. The first two events are temporally related. It was not possible to separate the two rain events for proper analysis since the first event had an impact on the runoff from the second event. The second runoff event contained elevated concentrations of sediment and nutrients compared to the first. As expected, there were additional runoff events from the cornfield. While all measures of N were low, measures of sediment and P from the cornfield were 2 to more than 6 times the concentration found in runoff from the bermudagrass field. When a runoff event occurred, both sediment and total P were of environmental concern. Sediment and total P from the corn/wheat rotation field was higher than that from the bermudagrass field. The corn/wheat rotation field produced more runoff events that the bermudagrass field.

The stilling pond provided little retention, and did nothing for water quality improvement, as operated. Retention time was too short to permit natural settling. The suspended clay solids in runoff waters, should they be released from impoundment basins, would be an environmental concern. Chemical treatment is likely to improve water quality for subsequent discharge. Three compounds were used: ferric chloride, ferric sulfate, and alum. All compounds were effective in TP removal below 1 ppm using basic chemical techniques. Alum was the most effective coagulant chemical. Pond design and operation should be explored for maximum improvement of water quality of runoff from phosphatic clay. Pond designs could be improved to reduce on-site channeling, and increase the pathlength for greater sedimentation and greater residence times.

This project focused on the agricultural aspects. Because of good landform design and proven crop production techniques upstream of the pond, runoff events were relatively few and low in volume. These conditions precluded exploration of pond management for improved water quality.

#### **INTRODUCTION AND BACKGROUND**

The project, *Managing Runoff Water Quality From Clay Settling Areas Used For Intensive Agricultural Production*, was based on work conducted by the Polk County Mined Lands Agricultural Research and Demonstration Project (1985-1995). Early in that project, water quality and nutrient losses due to erosion were identified as concerns as phosphatic clays were developed for intensive agriculture. The project presented here contained the elements originally proposed in the demonstration: a macrobed drainage system to prevent flooding of agricultural crops and a pond to retain runoff, allow eroded clays to settle, and serve as a potential watering source for agricultural operations with the field (Hanlon and others 1991).

#### STATEMENT OF SOURCE & MAGNITUDE OF PROBLEM

Phosphate mining in Florida has produced about 41,300 hectares (102,000 acres) of clay settling ponds with 9,300 hectares (23,000 acres) forecast to be constructed. Once waste clay is separated from the phosphatic ore matrix, clay is pumped to large impoundments (settling areas) as a 2% solid. With time, the clay settles out, and water is decanted for reuse in the mining process. After mining is complete, about 40% of the land surface is covered with clay settling areas. However, this percentage varies with the depth and thickness of the initial ore matrix, composition of the matrix, and constructed depth of the settling pond (Partney and Henderson 1992).

Approximately 24,280 hectares (60,000 acres) of the upper Peace River watershed is occupied by clay settling areas (S. Partney, Florida Department of Environmental Protection, Bureau of Mine Reclamation, personal communication, Oct. 27, 1994). The Peace River empties into Charlotte Harbor. Charlotte Harbor is a National Marine Estuary water body and is specifically under the auspices of SWIM (Surface Water Improvement and Management) planning (Livingston and others 1989). Additionally, the Southwest Florida Water Management District (SWFWMD) is developing plans to utilize the lower Peace River as a regional water supply for Sarasota and Charlotte Counties. Given these intentions and the high water quality standards required for environmental and human health, the quality of water runoff from clay settling areas is of great importance.

Presently, most reclaimed phosphatic clay sites are used for pasture, forestry, wildlife, or other low-intensity land uses. The Mined Lands Agricultural Research/Demonstration Project (MLAR/DP) is a jointly funded project of the Florida Institute of Phosphate Research, University of Florida, and the Polk County Board of Commissioners. The MLAR/DP has developed agriculturally intensive management strategies for reclaimed phosphatic clays (Peacock and Deck 1985; Hochmuth and others 1987; Baltensperger and others 1989; Hanlon and others 1991). While these clays are inherently fertile, have superior water holding characteristics compared to typical unmined sandy soils, and are agronomically productive, drainage has been identified as a

constraint to their utilization (Hanlon and others 1993). The MLAR/DP has developed certain management strategies to reduce this problem. One strategy includes land forming through construction of macrobeds, which increases surface drainage and permits more timely field access after storm events (Hanlon and others 1991a and b). Macrobeds are formed by shaping the phosphatic clay surface into a corrugated form with 1 to 2% slopes. To minimize clay movement during construction, macrobeds are usually 30 to 60 meters (100 to 200 feet) from crest to crest.

Increased surface drainage will increase runoff water volume. Runoff water may be impounded within another portion of the site (Hanlon and others 1991a) or, more appropriately, discharged off-site to contribute to the watershed. An associated potential problem is the increased transport of soil sediment with increased runoff. For water that is discharged from phosphatic clay ponded areas, water quality may be adversely affected by sediment content and increased phosphorus (P) concentrations.

As much as 70% of the phosphatic clay consists of particles of less than 2 microns. These clays are calcium saturated, which enhances flocculation compared to similar clays containing sodium. However, these clays typically contain from 1 to 4% organic matter (Jerez 1994), contributing little to secondary soil structure. Removal of phosphatic clay from the water column through sedimentation processes requires extended time. Most P in these runoff waters should be associated with the sediment (i.e., particulate portion).

# **REVIEW OF PERTINENT LITERATURE AND RELATED WORK IN PROGRESS BY OTHERS**

#### Effect of Agricultural Management Practices on Runoff Quality

The effect of agricultural management practices on soil erosion, water runoff, and water quality have been intensively studied due to national nonpoint pollution concerns (Edwards and others 1994, Mostaghimi and others 1992). As reported by Edwards and others (1994), greater runoff concentrations of nitrogen (N) and P were observed for the inorganic fertilizer than for the organic fertilizer application. The use of sludge on agricultural land under a no-till system is a viable alternative to chemical fertilizer use and control of N and P in runoff (Mostaghimi and others 1992).

Reduced tillage and other conservation tillage approaches have been shown effective in reducing nutrient losses due to subsequent reduction of erosion (McDowell and others 1980, McIsaac and others 1991). Additionally, sediment and nutrient concentrations in runoff waters can be reduced through the use of different vegetative covers (i.e., clover, ryegrass, and fescue) (Gross and others 1990, 1991; Croops and Bates 1993).

#### Model Application on Runoff and Water Quality

Modeling of agricultural conditions is an appropriate method for describing complex events and predicting the outcome given a much wider range of events with success. As with any stochastic or mechanistic model, there is an element of uncertainty with the prediction. Therefore, this project will try to verify a proven model, adapting this model to conditions found with crop production on phosphatic clays in Florida.

The curve number (CN) procedure was developed by the Soil Conservation Service to estimate direct runoff from storm rainfall. This information is needed for proper calculation of soil erosion, runoff water quality, and many other applications. The national database of curve numbers was built from runoff measurements (USDA-SCS 1972). Curve numbers represents soils, land use, antecedent soil moisture, and hydrologic conditions of a watershed (SCS TR-55 1986). Extrapolation of CN values from the national database to a specific field situation often causes errors in runoff volume estimates (Yoo and Touchton 1993). Therefore, the CN should be calibrated for phosphatic clay due to the special hydrologic conditions of clay settling ponds in Florida. The CN concept is used in several water quality models (e.g., GLEAMS, CREAMS, SWRRB, AGNPS, EPIC; Bingner and others 1989).

The CREAMS model (Chemical, Runoff, and Erosion from Agricultural Management Systems) has been widely used to evaluate runoff, sediment, pesticide, and nutrient losses for different soil and management conditions (Knisel 1993). Kenneth et al. (1990) studied nitrate concentrations in drainage waters from a potato production area on sandy loam soil by using the nutrient submodel of CREAMS in Quebec, Canada. They found that the CREAMS nutrient submodel over-predicted nitrate concentration in drainage water by 32 percent, but correctly predicted values in excess of the 10 mg NO<sub>3</sub>. N/L standard in all cases when the hydrology submodel value was greater than 0. The authors attributed lack of model precision due to accumulated errors within submodels and the need for more precise estimates within the nutrient submodel.

Another study conducted in Vermont compared simulated and observed monthly runoff, sediment, and P exports (Jamieson and Clausen 1988). The CREAMS model over-predicted exports for low-flow months and under-predicted exports during high-flow months. In all cases, coefficients of determination values remained between 0.78 and 0.90 except for the sediment prediction from one field.

After comparing annual runoff from 46 sites in the southern and Midwestern U.S. to predicted values, Smith and Williams (1980) concluded that the hydrology submodel was satisfactory. A study comparing the simulated results from CREAMS, SWRRB, EPIC, ANSWERS and AGNPS (Bingner and others 1989) showed that CREAMS and SWRRB produced results close to the measured values more often than the other models. The GLEAMS model (Groundwater Loadings Effect of Agricultural Management Systems) was developed as an extension of CREAMS and incorporates a component for both horizontal (runoff) and vertical (leaching) flux of pesticides and nutrients (Knisel 1992). The usefulness of this model is expected to be high, but no information is

available to verify the effectiveness of the nutrient component of this model for phosphatic clays in Florida.

#### **Enumeration of the Specific Project Goals**

The overall objective of this project was to enhance surface water quality discharged from agriculturally utilized phosphatic clay settling pond areas. Three specific objectives were:

To measure the effects of two selected soil management field-scale systems on runoff water quality as indicated by dissolved P, N, and sediment contents;

To determine the effectiveness of stormwater retention areas (stilling pond) for improvement of discharge water quality from phosphatic clay used for agricultural production;

To determine the effectiveness of chemical treatment of runoff waters before entering the stilling pond in enhancing sediment/nutrient retention and discharged water quality.

#### SMALL PLOT EXPERIMENT METHODS

#### **Small Plot Experiment, Green Bay Site**

Within phosphatic clay areas at the Green Bay site with established alfalfa, bermudagrass, or bare soil, 0.5- by 1-m plots were chosen with slopes ranging from 1 to 12%. Water was applied to each plot via a controlled droplet nozzle mounted vertically above the center of the plot at a constant height of 1.8 m. +/- 0.05 m. Pressure was maintained at 10 psi. +/- 1 psi. by regulated CO<sub>2</sub>. No change in water pH was found due to interaction with the CO<sub>2</sub> propellant. All runoff and sediment were collected during the timed water addition, which approximated a rainfall event of 2 inches (equivalent to a 10-year storm event, based upon Bartow weather data).

Both statistical regressions and GLEAMS (Groundwater Loading Effects of Agricultural Management Systems) model predictions were used to compare observed values with modeling values. Bermudagrass plots with 2 or 8% slopes were used for this initial calibration of the GLEAMS model because the standard for erosion models is a grassed surface.

The second small plot experiment was completed in partial fulfillment for a Masters of Science by Mr. D. Gao (Gao 1996). This experiment used a split plot design with a factorial arrangement of treatments using four replications. The objective was to determine the magnitude of erosion and N and P concentrations with and without ryegrass cover at 2 or 8% slope. As with the initial small plot work, 0.5- by 1-m plots

were chosen, and water was applied to each plot via a controlled droplet nozzle as described previously.

A sensitivity analysis of the GLEAMS model for N and P indicated that several parameters would require further investigation. Equations reported in the original literature concerning development of the GLEAMS model were used to predict mechanisms that might be changed to improve model prediction of some variables, such as P concentration in runoff from phosphatic clays.

Total runoff and sediment amounts were recorded, and N and P analyses (Figure 1) were performed on both sediment and runoff. Both statistical regressions and the calibrated GLEAMS model predictions were used to compare observed values with modeling values.

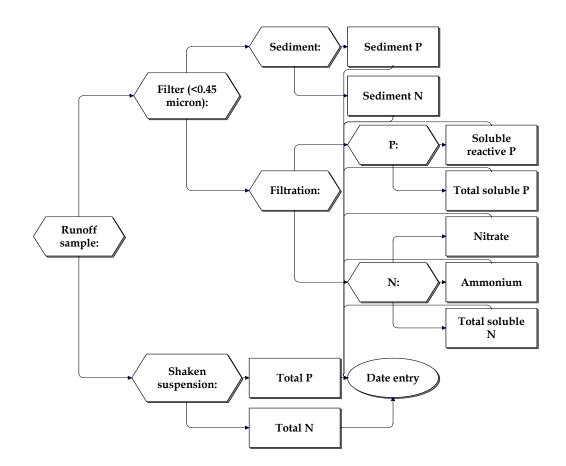


Figure 1. Analytical Pathway for Runoff Samples.

#### SMALL PLOT EXPERIMENT FINDINGS

#### **SMALL PLOT EXPERIMENT, FT. GREEN SITE**

Figure 2 shows that initial GLEAMS predictions were considerably higher than observed sediment values. As expected, the tabular values supplied with the GLEAMS model did not sufficiently represent erosion processes for phosphatic clay.

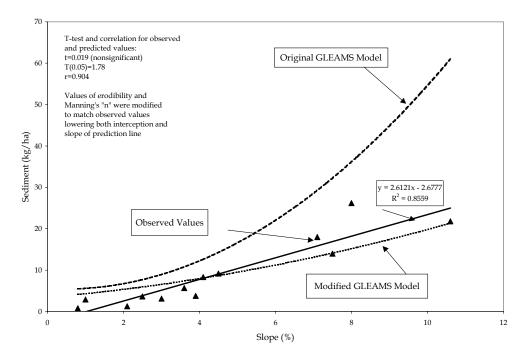


Figure 2. Initial and Calibrated GLEAMS Model Predictions with Observed Bermudagrass Sediment Values, Green Bay Site, 1995.

A sensitivity analysis of the model indicated that several parameters would require further investigation. Equations reported in the original literature concerning the development of the GLEAMS model were used to further highlight needed measurements of the phosphatic clay. This work produced a short list of parameters that were subsequently measured for phosphatic clay.

These measured parameters were entered into the GLEAMS model and compared to both observed small-plot values and linear regression (Figure 2). The calibrated GLEAMS model predicted sediment much better, and approximated the empirical linear regression.

The calibrated GLEAMS model was then used to predict sediment from both the bare soil (worst-case condition, Figure 3) and the alfalfa treatments (intermediate condition, Figure 4). The calibrated model did an excellent job of predicting sediment for the bare soil throughout the range of slopes. The GLEAMS model actually predicted

sediment value more accurately than linear regression because the model is mechanistic in nature, taking into account both chemical and physical properties of the clay.

The calibrated GLEAMS model was then compared to observed erosion on all bare phosphatic clay plots (Figure 3). Despite the observed variability, the calibrated model agreed with the empirical regression acceptably.

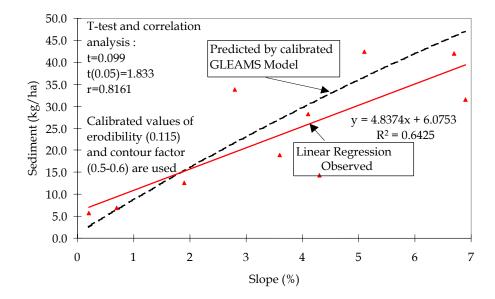


Figure 3. Predicted Bare Phosphatic Clay Sediment Values Using the Calibrated GLEAMS Model and Observed Values, Green Bay Site, 1995.

At the time of this small-plot work, the alfalfa stand was rapidly being replaced with the more aggressively growing bermudagrass. Only four satisfactory plots could be found with pure stands of alfalfa. The calibrated model predictably showed some deviation from these four points. The GLEAMS model is intended to estimate sediment and other runoff parameters using longer time periods than just one day and with more observations; however, the model did an acceptable job. These initial findings suggest that work with the model should continue.

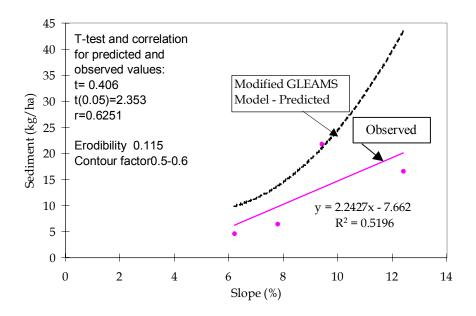
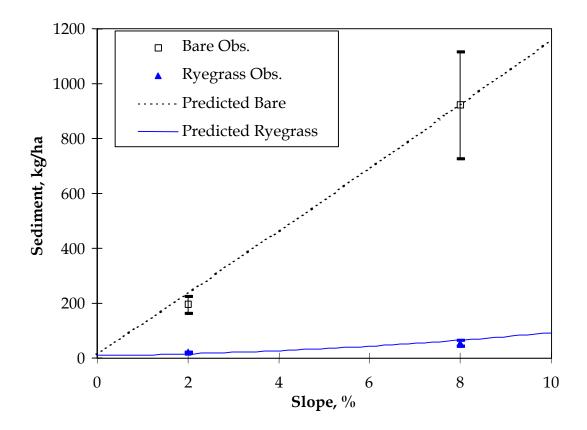


Figure 4. Predicted Sediment Values Using the Calibrated GLEAMS Model Compared to Observed Values from Phosphatic Clay with Alfalfa, Green Bay Site, 1995.

# MODELING RUNOFF DATA FROM SMALL PLOT EXPERIMENT, FT. GREEN SITE

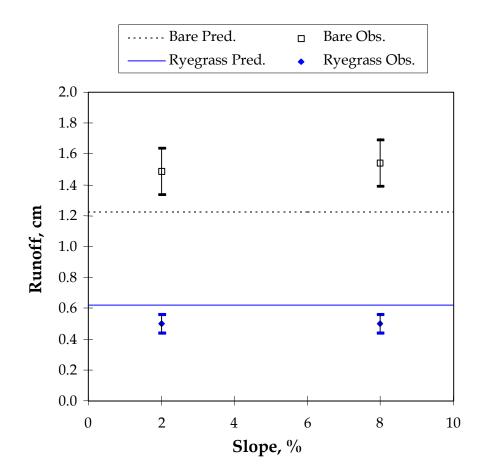
The calibration process, completed at the Green Bay site, improved GLEAMSmodel predictions of both sediment (Figure 5) and runoff (Figure 6) at the Ft. Green site. While runoff predictions are considered adequate in the uncalibrated model, the calibrated model did better in predicting sediment at measured slopes with or without cover. However, initial calibration work did not address N and P concentrations in runoff or sediment.



#### Figure 5. Predicted and Observed Sediment as a Function of Slope and Cover, Ft. Green Site, 1996. (Observed Data Presented with Standard Error Bars.)

Figure 6 demonstrates that the GLEAMS prediction for this single runoff event changed in magnitude as cover changed with selected slopes. However, the model did not produce predictions that fell within the variances observed from the small plots. It is important to consider that the model does best when predicting accumulated runoff, sediment, and other attributes with time. Therefore, this small plot work should be considered a challenging test of this semi-mechanistic model. In fact, the model did quite well. For example, the model predicted 1.2 cm of runoff from bare soil with changing slopes, and the observed value was 1.5 cm.

The apparent flat response (no y response to change in x value) of the model to increasing slope, regardless of cover, is a function of the fact that infiltration of water into this clay is very slow due to low measured saturated hydraulic conductivity. Therefore, water is modeled to produce equivalent amounts of runoff with a given cover regardless of slope. The model reflected observed measurements.



### Figure 6. Predicted and Observed Runoff from Small Plots as a Function of Slope and Cover, Ft. Green Site, 1996. (Observed Data Presented with Standard Error Bars.)

The model was sensitive to changes in cover and slope when predicting N and P in sediment (Figures 7 and 8). Even in this rigorous evaluation, the calibrated model predicted N and P in sediment values that were quite close to observed values (within observed standard deviations for the most part).

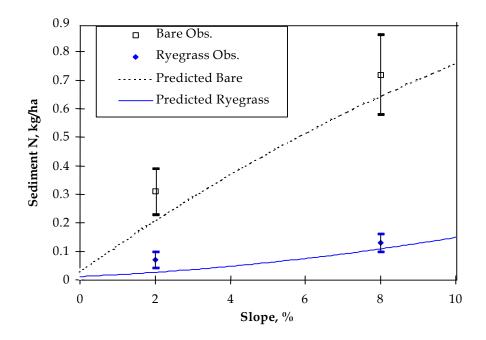


Figure 7. Predicted and Observed N in Sediment as a Function of Slope and Cover, Ft. Green Site, 1996.

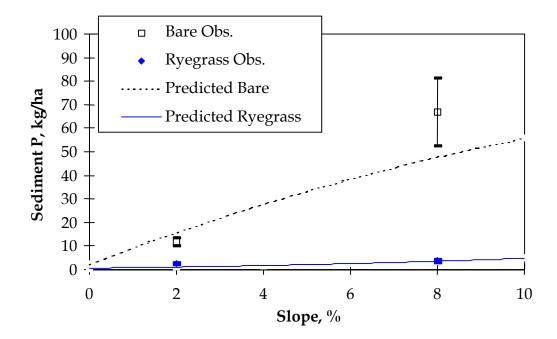


Figure 8. Predicted and Observed P in Sediment as a Function of Slope and Cover, Ft. Green Site, 1996. (Observed Data Presented with Standard Error Bars.)

However, predictions of N and P in runoff were not accurate, and in all cases were over-predicted. While it is interesting to note that observed runoff N and P values were considerably less than those predicted by the model, observed runoff-P values were quite high and of environmental concern. Recently, 0.015 ppm P has been identified as a concentration above which eutrophication becomes a concern. This concentration converts to 2 g ha<sup>-1</sup> (0.002 kg ha<sup>-1</sup>). Therefore, even at the 2% slope with ryegrass cover (best case scenario), soluble P in runoff (Figure 10) is a potential problem to oligotrophic environments.

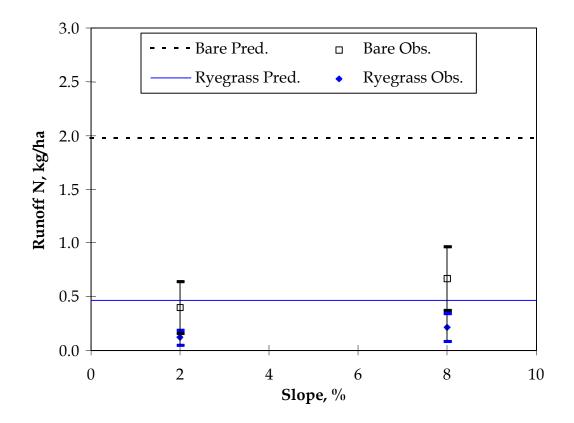


Figure 9. Predicted and Observed N in Runoff as a Function of Slope and Cover, Ft. Green Site, 1996. (Observed Data Presented with Standard Error Bars.)

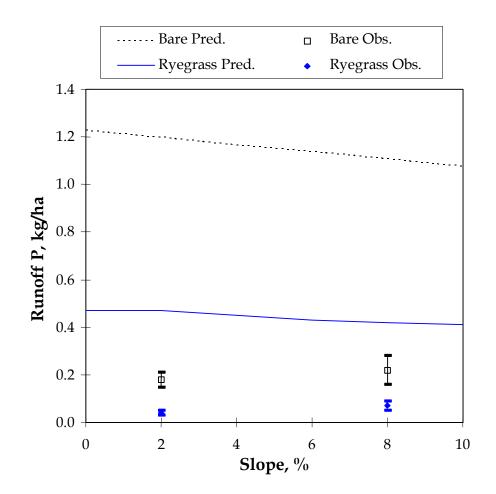


Figure 10. Predicted and Observed P in Runoff as a Function of Slope and Cover, Ft. Green Site, 1996. (Observed Data Presented with Standard Error Bars.)

Figure 11 shows the results of sensitivity tests on the calibrated GLEAMS model for N, and Figure 12 for P, in runoff. Each of these components has a major effect on predicted levels of N and P, and therefore indicate potential locations within the model to determine the cause for under- or over-prediction. For example, low estimates of porosity will lead to greatly over-predicted N in runoff. However, this model is designed to predict runoff and sediment values at the field scale.

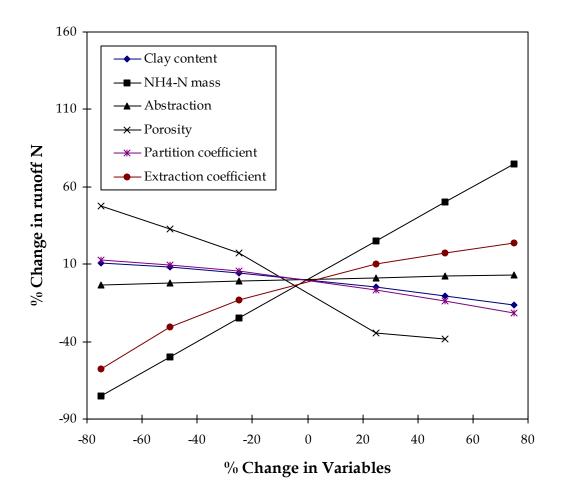


Figure 11. Sensitivity Analysis of GLEAMS Parameters for Prediction of N, Ft. Green Site, 1996.

The model should be expected to over-predict values within small plots, which is what was found concerning N and P in runoff. Exploration of the GLEAMS model mechanistic approach to runoff water quality is addressed in Mr. Gao's thesis (Gao 1996).

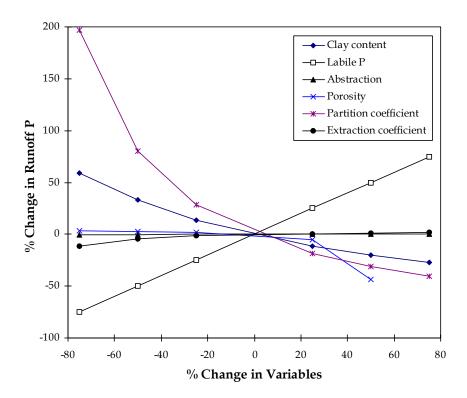


Figure 12. Sensitivity Analysis of GLEAMS Parameters for Prediction of P, Ft. Green Site, 1996.

#### LARGE FIELD MACROBED EXPERIMENT METHODS

#### **MATERIALS AND METHODS**

Two macrobeds, each approximately 1.2 ha in size and with slopes of 1-2%, were formed on a reclaimed clay settling pond at IMC-Agrico's Ft. Green Mine. Flumes with autosamplers and ultra-sonic distance sensors were installed at the drainage end of each macrobed. The eastern macrobed was planted to bermudagrass in May, 1996. The bermudagrass macrobed was mowed monthly to a 3-inch height to control weeds and promote grass growth. Bermudagrass was fertilized with 45 kg N ha<sup>-1</sup> (50 pounds N per acre) at planting and 27 kg N ha<sup>-1</sup> (30 pounds N per acre) in July, 1996. Fertilization was repeated in March, 1997 with 30 lbs/ac (pounds per acre) N as ammonium sulfate.

The second macrobed was clean tilled before planting temperate corn in July 1996. Plants were spaced to achieve about 54,000 plants  $ha^{-1}$  (22,000 plants per acre), and fertilized with 134 kg N  $ha^{-1}$  (150 pounds N per acre). Wheat was planted in rotation with the corn on December 13, 1996, with 54 kg N  $ha^{-1}$  (60 pounds N per acre) pre-plant fertilizer and an additional N application in March of 27 kg N  $ha^{-1}$  (30 pound per acre N). On April 11, 1997, wheat was harvested with the stover removed down to 3 inches. On June 4, 1997 the second crop of corn was planted (22,000 plants/acre). Fertilizer was incorporated at planting at the rate of 108 kg N  $ha^{-1}$  (120 pounds N per acre) as granular ammonium sulfate. The corn was harvested on September 15.

Rainfall was recorded using a Campbell Weather Station, in addition to temperature and wind speed. Programming automatically started and stopped the autosamplers based upon the depth of water in the flume (approximately 1 cm).

Soil samples were taken on a surveyed grid throughout each macrobed. Thirty samples were taken from each macrobed (0 to 5 cm depth) and analyzed for pH, and Mehlich-3 extractable Ca, Mg, K, and P. Both means and standard deviations were calculated.

Posts were surveyed on a 100-m grid throughout the pond, resulting in 20 locations. The posts were used as markers for monitoring plant colonization of the pond, and for determining sediment buildup. Two plant observations were taken – one in August 1996 and the second in April 1997.

A final survey of the macrobeds, connecting ditch, and pond inflow and outflow structures and pond was completed in June 1996 by NRCS personnel.

During the second year of the project the two agricultural fields produced five runoff events that could be sampled. While several samples were collected on July 3, 1997, the event was later determined to be a malfunction of the sensors and the data are not reported.

All runoff or discharge events were analyzed according to the flowchart presented in Figure 1. Results are reported in mg/L.

#### Filtration

A known quantity of sample is passed through a 0.45-µm filter. All P and N passing through the filter are in true solution. Material trapped on the filter is termed sediment.

#### Sediment

A known quantity of sample is passed through a 0.45- $\mu$ m filter. The filter and trapped material is dried at 105° C, and weighed. The difference in weight before and after filtration is a measurement of the sediment load (mg/L) of the sample.

#### **Sediment Phosphorus and Sediment Nitrogen**

Due to the small amount of sediment obtained by this method, no attempt to analyze the sediment was made. These values can be approximated by subtracting all measurements conducted on the filtered portion of the sample from unfiltered TP and TN values. For purposes of this report, only Sediment P was calculated.

#### **Soluble Reactive Phosphorus (SRP)**

A subsample of the filtered samples was analyzed using an ascorbic acid phosphomolybdenum blue color complex. Due to turbidity of the filtered samples and the nature of this colorimetric process, we expected an over-estimation of SRP. This test was included in this report for completeness. Reports in the literature discuss many problems with turbid samples and use of activated charcoal or other clearing solutions have introduced considerable errors. No attempt to correct for turbidity was made in this project.

#### **Total Soluble Phosphorus (TSP)**

The same subsample used for SRP was also analyzed using inductively coupled argon plasma spectroscopy (ICP). This process is less sensitive to turbidity, and will result in the soluble inorganic and organic fractions found in the filtered samples.

#### **Total Phosphorus (TP)**

An unfiltered sub-sample was digested using a standard perchloric acid digestion procedure. The resulting solution was analyzed for P using ICP. This method results in an estimate of all P in the sample, including solid, solution, organic, and inorganic fractions.

#### Nitrate (NO<sub>3</sub>–N)

Nitrate-N was determined in the filtered portion of the sample, and was analyzed for N using a standard colorimetric method.

#### Ammoniacal-N (NH<sub>4</sub><sup>+</sup>-N)

Ammoniacal-N was determined in the filtered portion of the sample, and was analyzed for N using a standard colorimetric method.

#### **Total Soluble Nitrogen (TKN)**

A filtered subsample was digested using a standard Kjeldahl nitrogen procedure. This method is an estimate of all soluble N in the sample, including both organic and inorganic fractions. The soluble organic N fraction can be estimated by subtracting the sum of  $NH_4^+$ -N and  $NO_3^-$ -N from TKN. This procedure was not done for this report due to low N values in the system.

#### Total Nitrogen (TN)

An unfiltered subsample was digested using a standard Kjeldahl nitrogen procedure. This method is an estimate of all N in the sample, including solid, solution, organic, and inorganic fractions.

#### **Mehlich-3 Extraction**

Soils were collected on a fixed-point basis with thirty sampling points located in each of the bermudagrass and corn/wheat rotation fields. Immediately following corn in both 1996 and 1997, six 2.5-cm by 15-cm soil cores were collected from within 1 m of each fixed point. Soil cores were air-dried, crushed using a stainless steel hammer mill, and screened to pass a 2-mm mesh opening. A soil volume of 2.5 cm<sup>3</sup> was extracted using Mehlich-3 solution and analyzed for Ca, Mg, K, and P by ICP (Hanlon and others 1998). Calculating the mean and sample standard deviation for each element within cropping system and year was used to summarize results.

#### **Use of Chemical Precipitation and Coagulation Techniques**

The use of chemical precipitation and coagulation techniques were investigated for the objective of reducing TP in mined-lands runoff waters. Three compounds were used: ferric chloride, ferric sulfate, and alum. After dosing, each compound acidified treatment waters. Calcium carbonate was used to readjust pH to initial water conditions (pH 7.2-8.0). The precipitant and coagulant compounds were allowed to settle by gravity and turbidities were measured. Total P and calcium were measured from water samples after settling.

#### LARGE FIELD MACROBED EXPERIMENT FINDINGS

Results of the Mehlich-3 extraction of soil samples (grid sampling, Table 1) revealed that there were no differences (P>0.05) between the samples in the two macrobeds. All samples were very high in Ca, Mg, K, and P. This uniformity was expected due to the use of this land for vegetable and agronomic crop production during the Polk County Mined Lands Agricultural Research and Demonstration Project (1985 through 1995). The high native fertility of the phosphatic clay is obvious.

Bermudagrass Macrobed									
	pН	Ca	Mg	Κ	Р				
		Ppm in	the soil						
Mean	8.07	6059	2823	368	605				
Std	0.06	196	111	45	48				
$\mathrm{Dev}^1$									
Corn Macı	obed								
	pН	Ca	Mg	Κ	Р				
		Ppm in	the soil						
Mean	8.09	6060	2900	363	516				
Std	0.02	96	84	36	49				
Dev									

# Table 1. Results of Soil pH (1:2 Water) and Mehlich-3 Soil Tests from the Macrobed Grid Sampling.

<sup>1</sup> Std Dev is the standard deviation of the 30 observations.

### AGRONOMIC DATA

The first crop of corn was harvested in the middle of October, 1996. Wheat was planted in rotation with the corn on December 13, 1996. On April 11, 1997, wheat was harvested with the stover removed down to 3 inches. On June 4, 1997, the second crop of corn was planted. The second crop of corn was harvested in the middle of September, 1997. Respective yields are presented in Table 2.

Crop	Subplot number	Stover (lb/ac)	Yield (bu/ac)
Corn 96	1	7,275	65
	2	5,807	62
	3	5,762	49
	4	6,013	77
	5	5,989	65
	Mean	6,169	64
Wheat 96/97	1	1,472	61
	2	1,481	59
	3	1,660	59
	4	1,043	60
	5	1,087	59
	Mean	1,349	60
Corn 97	1	6,219	45
	2	9,231	55
	3	6,638	43
	4	6,461	68
	5	7,797	66
	Mean	7,269	55

# Table 2. Corn and Wheat Yields Adjusted for Moisture (12%) from 5 Subplots.Stover is Reported on an Oven-Dry Weight Basis.

#### SEDIMENT ACCUMULATION IN THE POND

Twenty metal posts, placed throughout the pond in a grid fashion, were also used for monitoring of temporal changes in sediment accumulation in the pond. The elevations were taken at the beginning of the project in 1996 and at the end of 1997. Mean accumulation of sediment was 0.05 ft (0.6 inch).

#### WATER QUALITY

The Bermudagrass field had only three runoff events (Table 3). The first two events are temporally related. The second runoff event containing elevated concentrations of sediment and nutrients compared to the first event. Normally, a complete grass cover is quite stable and resists runoff or sediment transport. However, the soil surface was wetted completely by the July 14, 1997, event, directly affecting the runoff on July 16, 1997. Both unfiltered and filtered Total Kjeldahl Nitrogen (TKN-u, TKN-f) is quite low, as are ammoniacal- and nitrate-N concentrations. However, Soluble Reactive Phosphorus (SRP), Total Soluble Phosphorus (TSP), and Total Phosphorus (TP)

reflect changes in sediment concentration with time. While the TSP and TP values agree with the proposed fractionation described previously, the SRP appears to over-estimate this portion due to the turbidity of the samples.

As expected, there were additional runoff events from the cornfield (Table 4). The literature reports significantly more runoff and sediment from corn, compared to grass surfaces. While all measures of N were low, measures of sediment and P were twice to more than 6 times higher than that found in runoff from the bermudagrass field.

Design of the surface drainage system (1.5 to 2 % slopes with approximately 30m slope lengths), so-called macrobeds, has allowed considerable retention of precipitation. Evidence from small plot research (D. Gao, M.S. Thesis 1996) showed that precipitation events must exceed 50 mm before runoff occurs. This design also provided sufficient soil moisture for both the corn-wheat rotation and bermudagrass growth. Corn and wheat yields during this experiment are typical for production on phosphatic clay (MLAR/DP final report 1997). Yields are low compared to commercial production on undisturbed soils. However, input costs are considerably lower due to better N use efficiency and the inherent fertility of phosphatic clay compared to sandy soils in Florida.

Runoff from both the bermudagrass and corn/wheat rotation fields supplemented by additional runoff from adjacent phosphatic clay was sampled at the entrance to the stilling pond (Table 5). The conveyance ditch had a vegetative cover, mostly of Bermudagrass and weeds. However, the 1 to 2% slope of the channel was not expected to affect water quality. Only three measurable runoff events occurred at the inlet point to the stilling pond. As expected, the observed sediment and P fractions represent a composite of the concentrations reported on those dates for both fields (Table 3 and Table 4).

	<u>Min</u> 4.0	0.0	2.0		Min	1.4	0.3	1.0
	<u>Max</u> 8.0	26.0	7.0				3.7	
	<u>Std.</u> 1.7	6.0	2.1	Ы		-	0.8	-
TP	<u>Mean</u> 5.7			TKN-	Mean	1.8	1.3	1.4
	<u>Min</u> 3.2	0.0	1.6		Min	0.5	0.0	0.0
	<u>Max</u> 5.9	20.8	5.7		Max	1.3	0.5	0.0
	<u>Std.</u> 1.0	•		e-N	<u>Mean Std.</u>	0.3	0.2	0.0
TSP	<u>Mean</u> 4.2	4.7	3.1	Nitrat	Mean	0.8	0.4	0.0
	<u>Min</u> 5.1	0.0	2.4		Min	0	0	0
	<u>Max</u> 8.9			N-r	<u>Mean Std. Max M</u>	0.40.	0.0 0.	0.0 0.0
	<u>1.4</u>			ioniun	l Std.	0.1	0.0	0.0
SRP	<u>Mean</u> 6.7			Amn	Mear	0.2	0.0	0.0
	) <u>59.0</u>	0.0 (	0.20.0		Min	0.7	0.0	0.5
	<u>Max</u> 128.0 <u>5</u>				Max	7.3	1.0	0.7
<u>ent</u>	<u>Std.</u> 27.5	108.1	41.0				0.2	
Sedim	<u>Mean</u> <u>Std</u> 83.4 <u>27.5</u>			TKN-f	Mean	1.7	0.4	0.6
	<u>Obs.</u> 7				Obs.	7	15	S
	<u>Date</u> 14-Jul-97	16-Jul-97	8-Aug-97		Date	14-Jul-97	16-Jul-97	8-Aug-97

Table 3. Analyses of Runoff Water from Bermuda Grass Field, Bartow, FL, 1997, by Date.

1												1
	Min	0.0	0.0	3.0	2.0		Min		0.0	0.0	0.7	1.5
	Max	40.0	60.0	10.0	17.0		Max		3.1	3.4	16.8	2.3
	Std.	18.6	18.0	2.4	4.3				1.3			
TP	Mean	17.3	38.0	4.6	4.6	TKN-1	Mean		1.7	2.0	3.2	1.9
	Min	0.1	0.1	2.1	0.6		Min	0.0	0.0	0.0	0.0	0.5
	Max	28.4	42.4	7.6	13.5		Max	2.3	1.5	1.3	0.0	2.5
	Std.	13.6	12.9	1.8	3.5	N-9	Std.	0.7	0.8	0.4	0.0	0.7
TSP	Mean	12.9	27.8	3.7	3.5	Nitrate-N	Mean	0.8	0.8	0.8	0.0	1.4
	$\frac{\text{Min}}{0.0}$	0.0	0.0	2.9	0.8		Min	0.0	0.0	0.0	0.0	0.4
	<u>Max</u> 0.0	35.1	38.8	9.3	33.0	7			0.4			
	<u>Std.</u> 0.0	17.1	12.2	2.1	9.6	onium-N	<u>Std.</u>	0.1	0.2	0.1	0.3	0.3
SRP	<u>Mean</u> 0.0	16.5	29.0	4.9	7.2	Ammoni	Mean	0.2	0.2	0.1	0.1	0.9
	<u>Max</u> <u>Min</u> 545.0 0.0	0.0	0.0 (	30.0	19.0		Min		0.3	0.0	0.0	0.8
							Max		1.0	1.0	2.0	2.5
ent	<u>Std.</u> 128.5					ب	Std.		0.3	0.3	0.6	0.5
Sediment	<u>Mean</u> 30.3	218.7	698.0	64.9	75.5	TKN-f	Mean		0.7	0.4	0.4	1.3
	<u>Obs.</u> 18	9	8	6	7 11		Obs.	18	9	8	6	7 11
	$\frac{\text{Date}}{7\text{-Jul-97}^1}$	14-Jul-97	16-Jul-97	8-Aug-97	30-Sep-97 11		Date	7-Jul-97	14-Jul-97	16-Jul-97	8-Aug-97	30-Sep-97 11

Table 4. Analyses of Runoff Water from the Cornfield, Bartow, FL, 1997, by Date.

<sup>1</sup> Not all tests were completed due to low sample volumes.

	Min		11.0	1.0		Min		1.4	0.8
	Max		11.0	34.0		Max		1.4	1.5
	Std.		NA	12.4		Std.		NA	0.3
TP	Mean		11.0	13.6	TKN-1	Mean		1.4	1.1
	Min		7.8	0.6		Min	0.0	0.0	0.0
	Max		7.8	26.4		Max	0.2	0.0	0.5
	Std.		NA	9.7	N-	Std.	0.1	NA	0.2
TSP	Mean		7.8	10.4	Nitrate	Mean	0.2	0.0 NA	0.4
	<u>Min</u>	0.0	11.7	1.6		Min	0.0	0.2	0.0
	<u>Max</u>	0.0	11.7	29.0	Ż	Max	0.4	0.2	0.0
	<u>Std.</u>	0.0	NA	10.3	nium-	Std.	0.1	NA	0.0
SRP	<u>Mean</u>	0.0	11.7	12.5	<u>Ammonium-N</u>	Mean	0.0	0.2	0.0
	<u>Min</u>	0.0	188.0	6.0				1.0	
	Max					Max		1.0	0.7
<u>ent</u>	<u>Std.</u>	81.7	NA	104.4		Std.		NA	
Sedime	<u>Mean Std.</u>	27.2	188.0	161.2	TKN-f	Mean		1.0	0.4
	<u>Obs.</u>	6	1	5		$\mathbf{U}$	6	• •	S
	<u>Date</u>	7-Jul-97	14-Jul-97	16-Jul-97		Date	7-Jul-97	14-Jul-97	16-Jul-97

Table 5. Analyses of Runoff Water at the Pond Inlet, Bartow, FL, 1997, by Date.

97, by Date.	
nd, Bartow, FL, 1997,	
e Water from Poi	
ulyses of Discharg	
Table 6. Ana	

		Sediment	<u>ent</u>			SRP				TSP				TP			
Date	Obs.	Mean	Std.	Max	-	Mean	Std.	Max	Min	Mean	Std.		Min	Mean	Std.	Max	Min
4-Jul-97	10	322.6	159.0	538.0	$\overline{}$	18.5	7.7	27.4	0.0	14.3	6.8		0.0	18.5	8.9	30.0	0.0
6-Jul-97	17	292.4	102.8	460.0	115.0	15.1	4.7	22.3	6.7	12.7	4.5		5.1	16.1	5.6	26.0	7.0
8-Aug-97	0	63.0	73.5	63.0 73.5 115.0		4.2	4.6	7.4	0.9	2.9	3.4	5.3	0.5	3.0	4.2	6.0	0.0
		TKN-f				Ammc	<u>-mium</u>	Ż.		Nitrate	Z			TKN-L	, t		
Date	Obs.	Mean	Std.	Max		Mean	Std.	Max	Min	Mean	Std.			Mean		Max	Min
4-Jul-97	10	0.8	0.3	1.3		0.3	0.2	0.5	0.0	0.4	0.2	-		2.0		5.1	0.0
16-Jul-97 17	17	0.4	0.2	0.7	0.3	0.1 0.1 0.4	0.1	0.4	0.0	0.1 0.2	0.2	0.5	0.0	1.5	1.9	8.8	1.0
-Aug-97	0	0.3	0.0	0.3		0.0	0.0	0.0	0.0	0.0	0.0	-		1.0		1.2	0.7

#### **MODELING RUNOFF FROM LARGE MACROBEDS**

The data set collected from the research sites for bermudagrass, corn/wheat rotation, inlet to pond and outlet from pond covered a period of time from June 1997 through September 1997. Very short time of data collection (4 months), limited number of rain events with runoff, and some unexpected problems with the instrumentation caused periods of missing or unreliable data during this time. An attempt was made to validate the GLEAMS model for clay settling areas used for agricultural production using the data for this time period. Although the data collected were not sufficient to say that the results are statistically sound, some trends found for the modeling effort are noted below.

#### **Bermudagrass Macrobed**

The data set obtained from the macrobed planted in bermudagrass seemed to be the most complete and the best for the GLEAMS modeling effort. On this type of soils a significantly reduced antecedent moisture Condition I curve number can be expected due to cracking and swelling properties. The clay settling area cracks during dry periods which raises the initial abstraction prior to runoff. Abstraction is usually defined as all losses before runoff begins. Abstraction is highly variable but generally is correlated with soil and cover parameters. It includes water retained in surface depressions, water intercepted by vegetation, evaporation, and infiltration. As an example, on July 5, 1997, a rainfall of 1.47 inches produced only a 0.03 inch runoff. GLEAMS predicted a 0.29 inch runoff using a curve number of 86. On the following day, a 2.99 inch rainfall produced a 1.76 inch runoff, whereas GLEAMS predicted a 1.64 inch runoff. On the first day of rain, runoff water collects in the cracks and runoff is less than expected. On the following day, the clay is swelling shut and the storage in the cracks has been filled, thus runoff is at expected levels. GLEAMS does not model this initial abstraction on high shrink-swell clay soils. Care should be taken to include the initial moisture condition of the soils when modeling runoff.

Although individual runoff events are sometimes not well predicted by the model, due to shrink-swell proprieties of the soil, the model is much better predicting the overall runoff during the season. For the total period of data collection, from June 18, 1997, through August 8, 1997, the measured runoff was 3.24 inches and the GLEAMS predicted runoff was 3.31 inches. The graph of measured runoff versus GLEAMS predicted runoff shows that the daily-modeled runoff was not as close as the summed values for this period suggest.

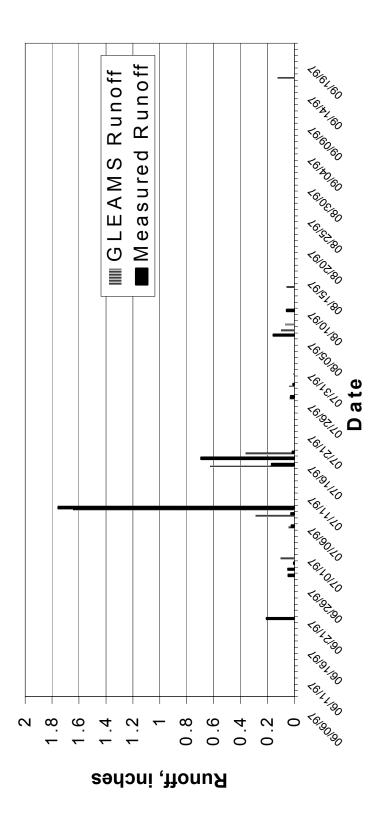


Figure 13. Predicted and Observed Runoff from Macrobed Planted in Bermudagrass.

Sediment yields for the bermudagrass covered bed were only measured and analyzed for three dates. On all three dates the measured sediment yield was larger than the sediment yield predicted by GLEAMS. The data are presented in Figure 14. On the only other date with sediment yield data, GLEAMS did not predict any runoff. Some other sediment data were taken, but the results were averaged across several days.

Nutrient data for these same dates were compared with predicted values from the GLEAMS model. The parameters compared were phosphate ( $PO_4$ ), nitrate ( $NO_3$ ), and ammonium ( $NH_4$ ).

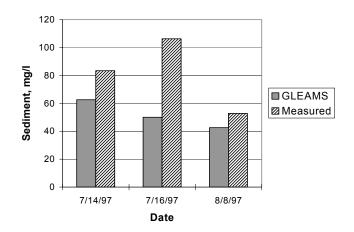


Figure 14. Predicted and Observed Sediment Concentration from Macrobed Planted in Bermudagrass.

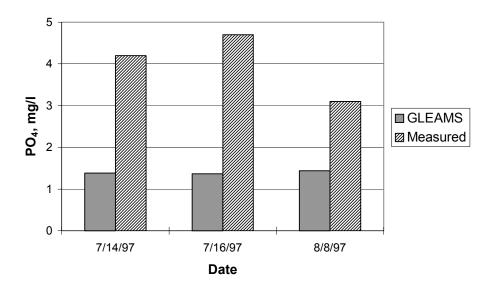


Figure 15. Predicted and Observed Phosphate (PO<sub>4</sub>) from Macrobed Planted in Bermudagrass.

Figure 15 presents the results of phosphate (PO<sub>4</sub>) analysis and modeling predictions. In all three events, the measured levels of PO<sub>4</sub> were higher than GLEAMS predicted values. As can be expected, PO<sub>4</sub> was mostly attached to the sediment particles (Figure 16). The amount of PO<sub>4</sub> was directly proportional to the amount of sediment present in the runoff from both fields.

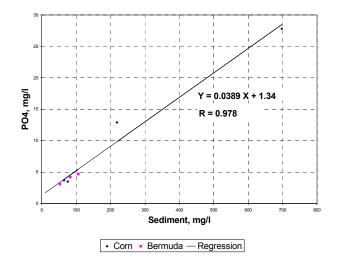


Figure 16. Phosphate Versus Sediment in the Runoff from All Experimental Plots.

Figure 17 presents the results of nitrate (NO<sub>3</sub>) analysis in runoff samples and modeling predictions. In this case, GLEAMS predicted concentrations were much higher than concentrations detected in the actual field runoff. This may be due to a model limitation since 1 ppm of NO<sub>3</sub> is the lowest value predicted larger than zero.

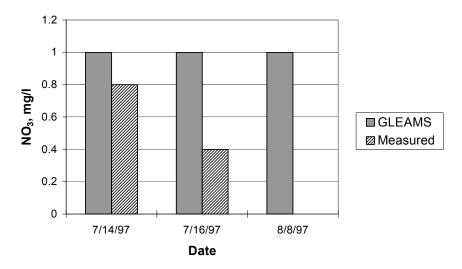


Figure 17. Predicted and Observed Nitrate (NO<sub>3</sub>) in the Runoff from the Macrobed Planted in Bermudagrass.

Figure 18 presents the results of ammonium (NH<sub>4</sub>) analysis in runoff samples and modeling predictions. Ammonium was detected in the water sample only during one of the runoff events at a very low level (0.2 mg/l). The GLEAMS model did not predict any ammonium in the runoff. The lowest level that can be predicted by the model is 1mg/l.

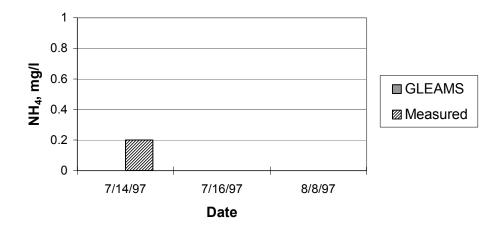


Figure 18. Predicted and Observed Ammonium (NH<sub>4</sub>) in the Runoff from the Macrobed Planted in Bermudagrass.

#### **Corn/Wheat Macrobed**

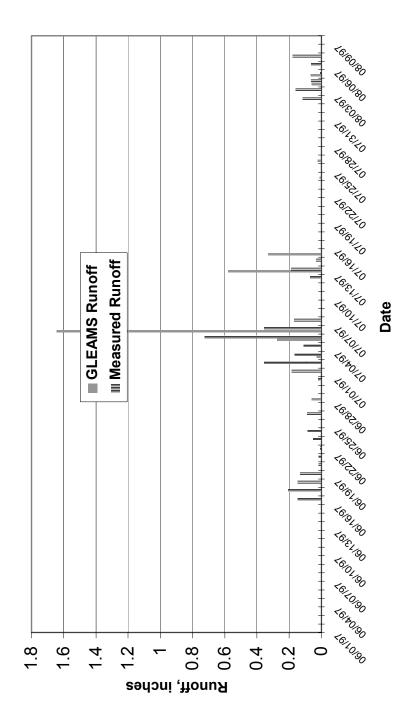
This data set had several inconsistencies. There were two days when runoff was measured and rainfall was not. This type of error could be caused by instrument drift, debris being blown into the flume and giving a false reading, or instrument setup error. We attempted to account for this type of error, but the presence of this type of error leaves doubt as to the accuracy of the measured data on those dates. The graph of measured runoff vs. GLEAMS predicted runoff is shown below (Figure 19).

The GLEAMS runoff prediction was much higher, especially when rain events were closely spaced in time. Small rain events that followed longer dry periods (for example between July 19 and August 8) resulted in predicted runoff much lower than the measured runoff. It is unclear if this was caused by measurement error, modeling error, or initial abstraction estimation error. It may also be a function of rain intensity.

Sediment concentration in the runoff water was measured for five events during the summer of 1997 and compared to GLEAMS-predicted sediment concentrations (Figure 20). Out of five events, in three cases the model predicted higher sediment concentrations than those measured in the actual runoff. On July 16, the actual sediment was more than seven times greater than predicted. This event closely followed the event on July 14 and the soil was saturated and without cracks. The three events with lower actual sediment concentrations were spaced farther apart in time. It can be speculated that some sediment was caught in the cracks and the runoff did not carry as many particles. The other possibility is that expanded, wet clay particles move easier. Further research would be necessary to investigate these hypotheses.

Nutrient data for these same dates were compared with predicted values by GLEAMS. The parameters compared were phosphate (PO<sub>4</sub>), nitrate (NO<sub>3</sub>), and ammonium (NH<sub>4</sub>). The data are presented in Figures 21, 22, and 23 respectively. With the exception of the first measured event, all measured PO<sub>4</sub> concentrations were higher than the values predicted by GLEAMS model. On July 16, when sediment concentration was above the predicted value, the measured phosphate was also much higher than the predicted value as can be expected. Differences in soluble P between predicted and observed values can be traced back to weakness of the soluble nutrient components in the nutrient sub-model as acknowledged by the model developers (Frere and others 1980).

Figure 19. Predicted and Observed Runoff from Macrobed Planted with Corn/Wheat.



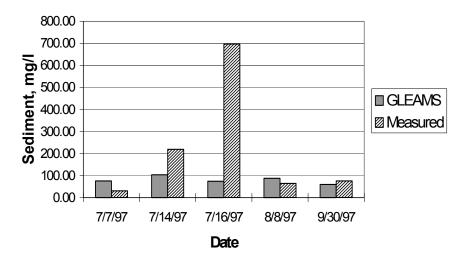


Figure 20. Predicted and Observed Sediment Concentrations from Macrobed Planted in Corn/Wheat.

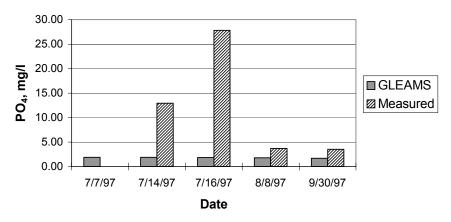


Figure 21. Predicted and Observed Phosphate (PO<sub>4</sub>) Concentrations from Macrobed Planted in Corn/Wheat.

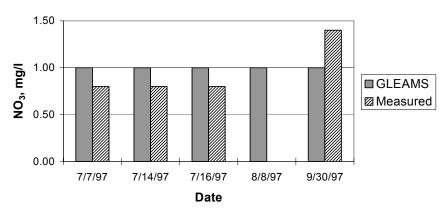


Figure 22. Predicted and Observed Nitrate (NO<sub>3</sub>) Concentrations in the Runoff from the Macrobed Planted in Corn/Wheat.

The predicted values for nitrate  $(NO_3)$  concentrations in the runoff from corn/wheat covered macrobed were very close to the concentrations measured at the field (Figure 22). The model predicts concentrations to the nearest mg/liter (ppm). As a result, the concentrations predicted are 1 mg/l. These results are consistent with those for the bermudagrass-covered macrobed.

For the corn/wheat macrobed, the predicted concentrations of ammonium (NH<sub>4</sub>) were much higher than the values detected in the runoff from the field, with the exception of the last event on September 30, when the observed concentration was higher than on any other event.

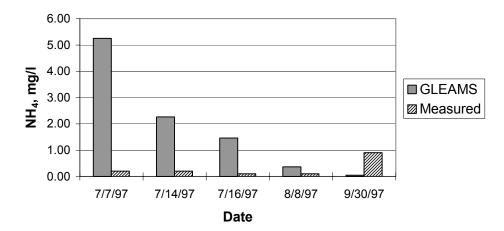
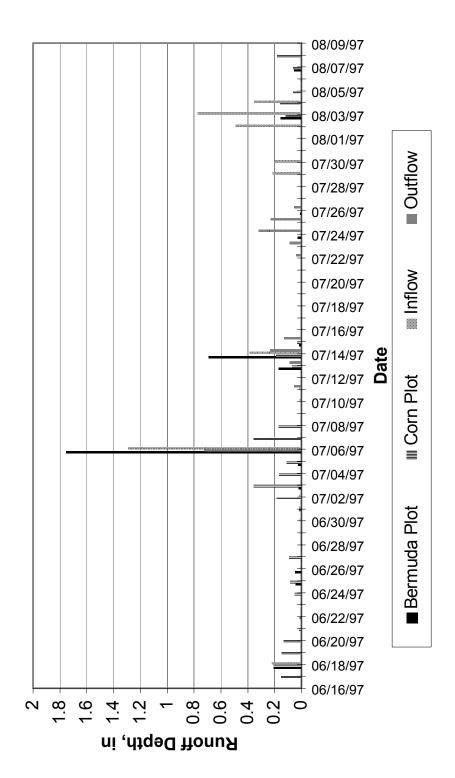


Figure 23. Predicted and Observed Ammonium (NH<sub>4</sub>) Concentrations in the Runoff from the Macrobed Planted in Corn/Wheat.

#### Pond

GLEAMS can only model one homogenous land-use with up to two channels and a pond. Since the research site has two different land use types (bermudagrass and corn/wheat rotation), GLEAMS could not directly model the pond outflow. An analysis of the water budget was expected to show that the volume of runoff for the bermudagrass and corn/wheat added together would approximate the amount of water flowing into the settling pond. The outflow from the pond was affected by pond size and was not a direct function of the inflow. Figure 24 presents all the components of this flow budget. The outflow from the pond is indicated in the lighter gray dotted line.





#### CHEMICAL TREATMENT OF SUSPENDED CLAY SOLIDS IN MINED-LANDS RUNOFF WATERS

The use of chemical precipitation and coagulation techniques were investigated for the objective of reducing total phosphorus (TP) in runoff waters from a reclaimed clay settling area used for agriculture. Three compounds were used: ferric chloride, ferric sulfate, and alum. After dosing, each compound acidified treatment waters. Calcium carbonate was used to readjust pH to initial water conditions (pH 7.2-8.0). The precipitant and coagulant compounds were allowed to settle by gravity and turbidities were measured (see Figure 25). Total P and calcium were measured from water samples after settling.

In all cases TP was reduced below 1 ppm. All compounds were effective in TP removal below 1 ppm using basic chemical techniques. Preliminary results indicated that alum was more efficient in TP removal than either ferric source. The treatment protocols did not affect pH nor calcium concentrations in the waters. Settling times (gravitational) of 30 minutes or less were generally suitable for visual removal of suspended solids. Greater settling times further improved solids removal.

The particle size distribution was calculated as mean, median, and mode. The mean represents the arithmetical mean particle diameter in the entire distribution in the size range 0.1-900  $\mu$ m. The median is defined as the particle diameter at which half of the distribution (50% percentile value) is larger and half is smaller. The mode is defined as the particle size that occupies the most volume in the distribution. Results are presented as volume percentages, which give a good interpretation of the space occupied by particles. Median data is often used to describe particle size distribution.

Suspended clay solids in clay settling area runoff waters contain high concentrations of phosphorus (P). Measurements of the turbidity (NTU) and particle size (mean or median) allow reasonable certainty in determining total P (TP):

TP = (0.197 x NTU x Mean) - (0.170 x NTU x Median)

with  $0.97 \text{ R}^2$  (R - linear correlation coefficient).

Turbidities of runoff samples ranged from 102 to 516 NTU. Mean particle sizes ranged from 0.846 to 2.945  $\mu$ m and the median particle sizes ranged from 0.533 to 2.585  $\mu$ m. Total phosphorus concentrations in these waters ranged from 9 to 56 ppm. These suspended clay solids in runoff waters, should they be released from impoundment basins, would be an environmental concern. For example, South Florida Water Management District established the Average Annual Concentration of Total P at the inflow structures to Lake Okeechobee not to exceed 0.18 mg/l (Lake Okeechobee SWIM Plan).

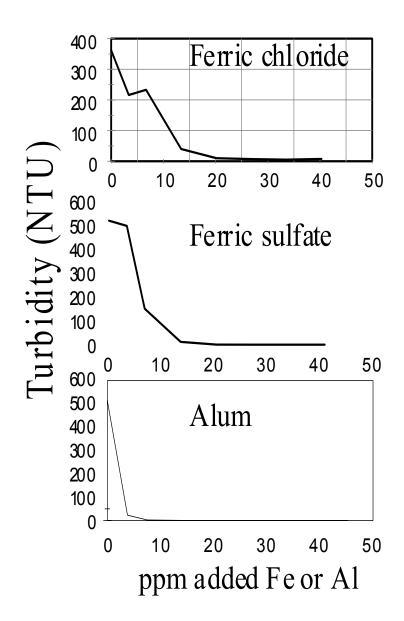


Figure 25. Turbidity Levels after Chemical Treatment.

#### SOIL PARTICLE SIZE AND DISTRIBUTION AT THE EXPERIMENTAL SITE

#### Objective

The objective was to determine the particle size and texture distribution of soils and sediments found in the growing areas and over-flow pond. Variations in particle size and texture may indicate the level or type of particle transport in the reclamation project.

#### **Materials and Methods**

Sixty soil core composites (5-6 cores, 0-6 inches deep) within the cropped reclamation project and twenty soil core composites within the over-flow pond were grid sampled. Samples (approximately 1000 g) were kept in field moisture conditions in plastic bags and sent to the laboratory within 72 hours.

In the laboratory, sub-samples of each core composite (approximately 400 g) were saturated with water and stirred until each sample had a liquefied paste consistency. This sample was used for particle size analysis. Particle size analysis was made on each sample in duplicate or until consistency in results (5%) was obtained.

1. The Coulter LS 130 particle sizing device was initialized and operated according to operating instructions (Coulter Corporation, 1994). The Fraunhofer model was used to calculate the particle size distribution (0.1 to 900  $\mu$ m).

2. Prior to analyzing the samples, a control with a known particle size distribution (Alcoa silica material) was analyzed every  $10^{th}$  sample to verify the consistency of the instrument. A blank (distilled water without sample) was included in each batch run to insure instrument "zeroing." All samples were duplicated and checked for consistency in results. If sample result variation in particle size fraction differed by more than 5%, the samples were rerun.

3. All samples were run in the same manner as the control. Each sub-sample was blended to be a representative sample. Obscurations between 45 and 55 % were used for each run, with a target obscuration count of 50%. If the obscuration was too low, additional sample was added. If the obscuration was too high, the sample was diluted by adding distilled water to the Coulter chamber.

The plastic bagged samples (approximately 600 g each) and moist prepared subsamples (250 ml vials) were frozen (-13°C) for storage. Moist sub-samples used for particle size analysis were composited for further testing and placed in storage (3°C).

#### **Reclamation Growing Area**

The average soil particle size across the growing area was 9.3 microns. The clay content was 14.7%; the silt content was 85.1%; and there was only 0.2% sand. The smallest mean particle sizes (Figure 26a) only ranged from 6 to 12 microns, but overall were relatively uniform. Particle size distributions for sand, silts, and clays were also relatively uniform across the growing area.

#### **Reclamation Overflow Pond**

The average soil particle size across the over-flow pond was 11 microns. The clay content was 12.3%; the silt content was 87.1%; and there was only 0.6% sand. The smallest mean particle sizes (Figure 27a) observed in the over-flow pond were found at the end of the pond flow stream, where settling of clay sized particles occur more commonly. Higher silt and clay-sized fractions were found in these areas (Figures 27b and 27c). This was apparent in Figure 27d, which shows higher sand deposits where flows enter the pond. The larger particles settle faster and are thus found nearer to the inflow.

Runoff overflow ponds are currently used to capture sediments and nutrients. However, channeling within these ponds may lead to very short residence times, too short to remove P-bound sediments by gravity alone. The use of ferric compounds or alum to precipitate and coagulate solids and soluble phosphorus has merit if the over-flow ponds discharge waters to the outside.

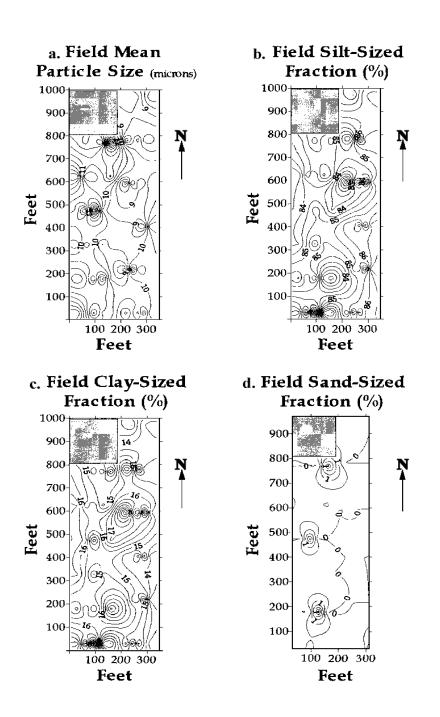


Figure 26. a. Mean Particle Size, b. Silt (2-64 μm) Content, c. Clay (0-2 μm) Content, and d. Sand(>64 μm) Content of Sediments in the Reclamation Growing Area.

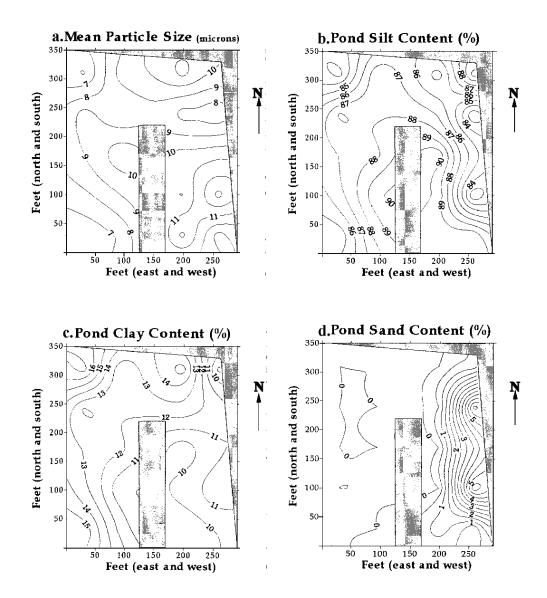


Figure 27. a. Mean Particle Size, b. Silt (2-64 μm) Content, c. Clay (0-2 μm) Content, and d. Sand (>64 μm) Content of Sediments in the Over-flow Pond.

#### CONCLUSIONS/RECOMMENDATIONS

The macrobed design worked well to permit intensive cropping (corn/wheat rotation) or pasture production (bermudagrass), and harvest most rainfall events for plant use.

While numerous precipitation events occurred in both years, most water was retained on site (no runoff).

Crop growth and yield were consistent with previous production on phosphatic clay, indicating that water supply was adequate.

When a runoff event occurred, N forms were below regulatory concern, and demonstrated that use of UF-IFAS fertilization recommendations will result in little loss of N from phosphatic clay.

When a runoff event occurred, both sediment and TP were of environmental concern.

Sediment and TP from the corn/wheat rotation field was higher than that from the bermudagrass field.

The corn/wheat rotation field produced more runoff events that the bermudagrass field.

The stilling pond provided little retention, and did nothing for water quality improvement, as operated.

Retention time was too short to permit natural settling. Chemical treatment is likely to improve water quality for subsequent discharge. Alum was the most effective coagulant chemical. The data indicate that small chemical additions of alum will remove >99% of the total P in the system. Field scale research on chemical treatment should be considered.

Pond design and operation should be explored for maximum improvement of water quality of runoff from phosphatic clay. Pond designs could be improved to reduce in-site channeling, and increase the pathlength for greater sedimentation and greater residence times. More research on various pond designs and their effectiveness in sediment removal is recommended.

This project focused on the agricultural aspects. Because of good landform design and proven crop production techniques upstream of the pond, runoff events were relatively few and low in volume. These conditions precluded exploration of pond management for improved water quality.

Findings related to water quality in the large field trial were consistent with the findings of small plot research conducted earlier.

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Appendix A

### POND SURVEY DATA

Pin #	Water Depth	Common Name	Height	Clock Loc.	Distance from Pin
	inches		inches		inches
1	.5	Sesbania	48	12:00	24
		2 dogfennell	12	2:00	6
		1 dogfennell	12	4:00	18
		1 vaseygrass	9	3:00	12
		30 willows	6-9	all over	
		1 bahia	12	3:00	36
		1 bahia	12	10:30	12
2	3.5	1 vaseygrass	36	11:00	24
		2 willows	12	12:00,12:30	24
		1 willow	18	9:00	12
		1 willow	6	3:00	16
3		1 dogfennell	18	9:30	24
		1 vaseygrass	36	5:00	6
		1 marshepper smartweed	10	5:00	16
		1 hyssop spurge	10	1:00	8
4		8 vaseygrass	12	3:00	1,8
				4:00	16
				5:00	18
				9:00	14
				10:00	6
				11:00	12
				1:30	12

## Table A-1.Results of First Survey of Colonizing Plants in the Pond, Ft. Green,<br/>August, 1996.

		1 southern crabgrass	8	4:30	6
5		1 vaseygrass	48	3:00	24
		1 vaseygrass	18	4:00	24
		3 vaseygrass	36,24,36	6:00	12,24,36
		1 vaseygrass	12	9:00	18
		1 vaseygrass	36	10:00	18
		1 vaseygrass	36	12:00	24
		2 vaseygrass	36,12	1:00	12,36
6		7 sesbania	24	9:00	24
		1 vaseygrass	36	10:00	24
		1 vaseygrass	12	10:00	4
		4 vaseygrass	36	12:00	6,12,18,24
		1 vaseygrass	60	3:00	36
		1 vaseygrass	60	4:00	36
		1 vaseygrass	48	4:00	12
		2 vaseygrass	48	6:00	24,36
		1 vaseygrass	48	8:00	24
7		1 crabgrass photo/3	12	1:00	24
		1 vaseygrass	8	5:00	12
		2 vaseygrass	8	7:00	12,18
		1 vaseygrass	6	8:00	6
8		1 sesbania	50	4:00	24
		1 vaseygrass	30	12:00	16
_		1 willow	12	6:00	16
		1 vaseygrass	16	10:00	18
9	8	No weeds			
10	10	No weeds			

11	1 willow	6	4:00	6
	1 sesbania	36	5:00	36
	2 vaseygrass	6,8	6:00	24,36
	1 vaseygrass	36	7:30	18
	2 willows	8,4	10:00	6,12
	1 vaseygrass	12	10:00	24
	1 vaseygrass	12	12:00	30
	1 vaseygrass	36	1:00	24
	1 aeschynomone	8	2:00	18
	1 vaseygrass	36	3:00	30
12	1 vaseygrass	36	12:30	6
	1 vaseygrass	6	3:00	12
13	1 spurge	8	12:00	12,16
	3 spurge	6	1:00	12,18,24
	1 sesbania	30	1:30	40
	5 vaseygrass	4,8,6,12,16	3:00	4,12,18,24,36
	4 vaseygrass	8	4:00-5:00	16-32
	1 vaseygrass	8	6:00	14
	1 vaseygrass	6	7:00	12
	1 vaseygrass	6	8:30	6
	1 vaseygrass	8	3:30	18
	1 vaseygrass	6	11:00	12
	1 vaseygrass	16	12:00	18
	2 spurge	4	3:00	8,12
14	1 sesbania	72	6:30	30
	1 sesbamoa	50	10:00	30
	2 vaseygrass	12,36	1:00	8,12

	1 vaseygrass	16	3:00	24
	1 vaseygrass	20	4:30	16
	3 vaseygrass	12,12,24	6:00	8,16,24
	1 vaseygrass	16	8:00	18
	1 vaseygrass	16	8:30	8
	1 vaseygrass	16	10:00	4
15	bare spot		12:00-1:00	
	bare spot		3:30-4:30	
	rest-vaseygrass			
16	3 sesbania	84	6:00	36
			8:00	24
			9:30	24
	1 sesbania	54	1:00	24
	understory of crabgrass			
	1 dogfennell	12	6:00	24
17	2 crabgrass	6	1:00	12,18
	1 crabgrass	6	9:00	4
	1 crabgrass	6	6:00	12
	1 crabgrass	6	4:00	24
	1 crabgrass	6	5:00	18
	1 vaseygrass	8	1:00	8
	1 vaseygrass	10	2:30	12
	4 vaseygrass	6	4:00	4,8,16,21
	1 vaseygrass	8	6:00	24
	3 vaseygrass	6	7:00	8,12,24
	1 vaseygrass	24	8:00	30

	1 vaseygrass	8	8:30	12
	1 vaseygrass	24	9:00	36
18	1 vaseygrass	40	12:00	24
	1 vaseygrass	40	1:00	30
	1 vaseygrass	8	1:30	18
	1 vaseygrass	12	2:00	16
	1 vaseygrass	40	2:30	12
	1 vaseygrass	24	3:00	10
	1 crabgrass	10	4:00	24
	1 vaseygrass	16	3:30	30
	1 vaseygrass	24	5:00	12
	1 vaseygrass	16	5:30	16
	1 vaseygrass	48	8:30	30
	2 vaseygrass	8	10:30	12,16
	1 vaseygrass	10	11:00	24
	1 vaseygrass	24	11:30	30
19	1 sesbania	12	1:00	10
	1 vaseygrass	36	2:00	8
	1 vaseygrass	12	4:30	12
	1 vaseygrass	12	6:00	36
	1 vaseygrass	24	8:00	24
	1 sesbania	24	9:00	30
	1 crabgrass	16	9:00	12
20	1 dogfennell	20	3:00	4
	1 vaseygrass	24	4:30	12

Pin #	Weed Common Name	Weed Ht. in In.	Clock Loc.	Distance from Pin in In.
1	mock Bishop's weed	8,4,4	7:00	27,27,33
		6	4:00	33
		8	1:00	32
1	dog fennell	14	5:00	29
		10	11:00	12
		10	12:00	5,12
		21,26,32	9:00	3,9,12
		10	8:00	30
		14	4:00	16
	willows	14,14,11,14,14,14	2:00	3,13,16,16,22,26
		9-14	11:00	9,11,14,14,16,16,17,17,1 7,17,20,21,22,23,23,23,2 3,25,26,26,26,28,29,30,3 0,30,31,31,32,32,33,33,3 3,33,33,35,35,35
		5,5,7,5,8,12,7,7,11,7,1 2,5,4,6,6,14	10:00	10,11,14,15,17,18,20,20, 21,21,27,31,31,33,35,35
		20	12:00	2-36
		18	6:00	1-27
		8,10,5,14,16,11,9,16	3:00	4,7,8,15,16,20,.23,24
		8,18,9,8,13,12,8,2	9:00	3,3.5,6.5,17,20,22,25,27
		14,13,14,14,11,13,14,8 ,14,4,16	8:00	10,10,13,13,16,18,21,21, 21,23,25
		9,11,12,12,9,7,7,7,7,9, 7,7,8,4,4	7:00	11,12,13,16,17,22,23,24, 25,26,27,27,33,33,33
		8,8,8,8,4,4,7,7,8,7,8,5, 4,10,4,5,4,7,8	5:00	10,12,14,15,17,21,23,23, 24,25,25,26,27,27,27,31,

# Table A-2. Results of Second Survey of Colonizing Plants in the Pond, Ft. Green, April, 1997.

		4,10,4,5,4,7,8		21,31,35
	marsh aster	6	5:00	9,20
		4,4,4,8,4,4	12:00	15,18,24,25,26,31
		6	4:00	16
	vaseygrass	9,6,	3:00	10.5
		20,10	3:00	35
		10,8	3:00	18
		8,6	7:00	30
	ragweed	6	6:00	28
		4	7:00	22
		5	4:00	31
	spurge	6	7:00	3
	peppergrass	11	12:00	22
		8	4:00	21
2	dogfennell	14	12:00	27
	mock Bishop's weed	8	12:00	1
		9	6:00	3
		6,6	9:00	24,2
		8	1:00	25
		4,5,3,13,8	12:00	10,23,26,34
		10,5,12	3:00	27,28,30
		3,4,3	2:00	13,24
	willow	16,17,18,13	12:00	19,20,23,27
		11,15,16,17,9,9,9,11,9, 6,9,9,11,17,9,9,6,9,11	6:00	22,22,24,28,30,30,30,31, 31,31,32,32,32,32,34,34, 34,34,34
		14	1:00	16
		32,5	9:00	11,17

		12-18	5:00	28,30,30,30,31,31,32,32, 32,32,33,33,34,34,35,36
	marsh aster	7	12:00	31
		5	9:00	25
		6,10,16	7:00	21,21,33
		4,6,3	8:00	24,28,35
		4,7	1:00	30,33
	vaseygrass	4	9:00	33
		10	11:00	22
3	dog fennell	34	9:00	25
	vaseygrass	6	5:00	4
		8	9:00	20
		6	2:00	19
	marsh aster	5	5:00	10
4	vaseygrass	4,6,5	6:00	18,26,36
		4	7:00	25
		2	8:00	25
		5	9:00	13
		57	10:00	16
		7	11:00	11
		6,10	2:00	21,24
		4	2:00	12
		4,4	4:00	9,20
		4,4,4	5:00	18,26,33
	bermuda	6	7:00	25
		6	8:00	33
		4	9:00	13-25

		6	10:00	10-26
		12	11:00	19-25
		10	12:00	16-20
		10	1:00	8-18,26-35
		8	3:00	10-20
		8	3:00	28,32-36
		10	4:00	18-36
		8	5:00	26-36
5	dogfennell	11,10	6:00	9,20
		14,16	2:00	15,29
		10	1:00	32
		7,8	4:00	13,23
		9	5:00	10
	cogongrass	15,22,22	6:00	16,22,27
		12	8:00	25
		14	10:00	13
		16,12,14,14	11:00	14,27,29
		14	12:00	16-29
		16-22	2:00	13-30
		30	3:00	21-36
		16,16,17	5:00	20,23,33
	bushy bluestem	14	6:00	4
		13,13	7:00	22,34
		10,10	9:00	25,13
		12	12:00	34
		10,8	2:00	6,31
		10	3:00	4

		22	4:00	33
		10	5:00	19
	vaseygrass	6,4,12	6:00	12,21,36
		8	8:00	25
		7	9:00	14
		12	10:00	32
		8,10	11:00	14,32
		10	3:00	18-27
	primrose willow	3	9:00	34
	phasey bean	10	6:00	5
	bermuda	8	10:00	16
		12	11:00	15
6	dogfennell	15	12:00	16
	vaseygrass	15	12:	1-30
		7	12:00	25
		9	3:00	28
		18,18	4:00	9-16,26-35
		13,16	5:00	31,17
		19	6:00	13-36
		17	7:00	24-36
		7,9	8:00	25,33
		17,13	9:00	31,6
		21,12	10:00	26,31
	bushy bluestem	10	1:00	8
		11	3:00	7
	bermuda	13	3:00	17-24

		14	4:00	22-29
		8	9:00	7
	phasy bean	5	3:00	14
		10	4:00	33
		12	5:00	33
		4,6	6:00	23-25
7	Vacavarass	6,4	12:00	33,23
/	vaseygrass	5	12:00	6
		4,4	2:00	14,32
		4,6	4:00	20,27
		6	5:00	33
		6,7,9	6:00	9,24,32
		4,5,9,7	7:00	9,19,30,33
		7,9,7	8:00	13,21,34
		6,5	10:00	22,32
		6,6	11:00	22,34
	bermuda	9	1:00	11-21
		10	10:00	22-29
	phasey bean	4	7:00	26
8	vaseygrass	8	12:00	19
		6	11:00	33
		8-4	10:00	17-36
		6	6:00	33
		4,5,15	6:00	17,30,36
		4	2:00	28
	willow	10	6:00	6
9	marsh aster	16	9:00	20

		6,26	4:00	14,27
		10,8	3:00	15,25
		10,8,18	2:00	14,25,34
	horse weed	16	12:00	15
		18	1:00	22
		21	6:00	20
	mock Bishop's weed	10,10,10	12:00	18,18,22
		10	9:00	5
		6	2:00	10
	Florida beggar weed	10,8,25	3:00	23
		28	11:00	16
	vaseygrass	3,6,4	9:00	9,14,27
		2	6:00	8
		4	2:00	20
		5	1:00	23
		11	1:00	27
	dogfennel	4	6:00	21
		6,6,7	3:00	11,18,23
10	marsh aster	20,4,20	12:00	12,18,36
		12,16	1:00	28,29
		13,7,6	2:00	24,28,34
		12,7,2,4,2,3,4,4,15,6	3:00	10,12,15,17,19,22,23,28, 30,33
		9,5,4,4	4:00	15,19,28,31
		10	5:00	34
		12,16,3,16,12,25,9	6:00	11,19,19,24,28,33,35
		5,14,15	7:00	11,24,33

		16,14,11	9:00	20,24,28
		10,18,15,13,14	10:00	14,25,25,33,33,
		13,16,19	11:00	8,21,32
	vaseygrass	7	7:00	34
	marshpepper smartweed	10	10:00	13
11	vaseygrass	5,3,9	6:00	20,33,33
		28	12:00	30
		12	3:00	26
		8	2:00	33
		8	1:00	21
		10,5	8:00	18,28
		6	11:00	21
	sea myrtle	16	6:00	22
	willow	7	12:00	34
		15	2:00	3
		9	5:00	5
		13,5	11:00	6,12
	marsh aster	3,3,5	2:00	5,13,23
12	vaseygrass	10	12:00	
		35	1:00	
		4	3:00	
		3	7:00	
		4	12:00	
13	vaseygrass	4	6:00	
		6,4	11:00	15,28
		4,4	10:00	20,29
		4,4	9:00	19,31

	4,4	8:00	7,33
-	4,6,4,4,4	7:00	12,21,24,29,34
	15	5:00	33
	4,4,4	4:00	16,19,26
	4,4		14,33
vaseygrass	10,14	7:00	30,21
	14,9,9	5:00	15,27,29
	6,6	3:00	20,31
	6,6	2:00	30,35
	6,6	1:00	28,28
	9,13	9:00	20,33
	10	10:00	32
	10,6	11:00	25,33
	7	12:00	26
bushy bluestem	6	12:00	20
bushy bluestem	12,12	12:00	6,30
	12,12	1:00	25,31
	8,11	2:00	12,25
	12,14,14	3:00	18,22,30
	18,18	4:00	14,27
	16	5:00	32
	15,15	6:00	19,32
	10	8:00	26
	10	9:00	4-19
	10	10:00	33
	12	11:00	10-23
vaseygrass	25	10:00	28
	Image: state stat	15         4,4,4         4,4         vaseygrass       10,14         14,9,9         6,6         6,6         9,13         10         10,6         7         bushy bluestem         6         bushy bluestem         12,12         8,11         12,14,14         18,18         16         10         10         10         12,12	4,6,4,4,4         7:00           15         5:00           4,4,4         4:00           4,4         4:00           4,4         7:00           10,14         7:00           14,9,9         5:00           6,6         3:00           6,6         2:00           6,6         1:00           9,13         9:00           10         10:00           10,6         11:00           7         12:00           bushy bluestem         6         12:00           bushy bluestem         12,12         12:00           12,12         1:00         12:00           13,18         4:00         13,18           4:00         16         5:00           10         15,15         6:00           10         9:00         10         10:00           10         9:00         10         10:00           10         10:00         10:00         10:00

		9	8:00	29
		9	12:00	16
		19	11:00	33
16	vaseygrass	12	6:00	9-30
		12	7:00	10-36
		12	8:00	9-36
		12	9:00	8-36
		12	10:00	8-36
		12	11:00	7-36
		7,8,8	5:00	4,26,31
		11	4:00	23-36
		15	3:00	7-36
		11,15,15,17	2:00	9,23,29,34
		14,10	1:00	19,34
		8,14	12:00	3,24-36
	caesar weed	6	10:00	31
		4	11:00	18
	dog fennel	21	6:00	27
17	vaseygrass	5,5,7,10,10,4	6:00	8,8,12,16,19,28
		10,4,4,4,4	7:00	7,11,19,25,30
		8,6	8:00	11,23
		7,6	9:00	12,26
		5,3	10:00	29,35
		6,4	12:00	12-31
		9,6,3	1:00	13,19.29
		7,4,4	2:00	6,10,12
		5,5,	3:00	9,28,32

		6512	4:00	1 22 25 22
		6,5,4,3		4,22,25,33
ļ		9,5,4	5:00	10,15,13
	bermuda	6	7:00	21
		3		
		5,6,5	1:00	16,23,29
18	vaseygrass	14,14	12:00	24,24
		7	6:00	24
		18	8:00	32
		10	10:00	10,15,22,25,28,33
		10	5:00	13,25
		7,13	4:00	19,27
		12	3:00	14
		7,12	1:00	17,34
		9	11:00	27
	phasey bean	8	11:00	27,16
19	vaseygrass	6,5	5:00	12,30
		5,5,6	1:00	8,17,26
		26	6:00	27
		9	3:00	21
20	dog fennel	31	3:00	6
	vaseygrass	10	12:00	33
		10	2:00	33
		15	3:30	33
		10	5:00	8
		8	7:00	30

Pin #	Initial Elevation (ft)	Final Elevation (ft)	Elevation difference (ft)
1	41.24	41.26	-0.02
2	41.14	41.20	-0.06
3	41.36	41,52	-0.16
4	42.14	42.22	-0.08
5	42.84	42.94	-0.10
6	42.83	42.92	-0.09
7	41.74	41.61	0.13
8	41.54	41.50	0.04
9	40.79	40.90	-0.11
10	40.48	40.64	-0.16
11	40.33	40.29	0.04
12	40.64	40.74	-0.10
13	41.98	41.97	0.01
14	41.04	41.15	-0.11
15	42.28	42.43	-0.15
16	40.83	40.87	-0.04
17	41.17	41.20	-0.03
18	41.24	41.13	0.11
19	40.59	40.57	0.02
20	39.64	39.71	-0.07

## Table A-3. Initial (May 24, 1996) and Final (Oct. 16, 1997) Elevations in the Sedimentation Pond.

	х	у	Avera	age Values	(µm)		Clay	Silt
Sample	(ft)	(ft)	mean	median	node	<2µm	2-64µm	>64µm
1	220	30	7.79	5.08	4.39	15.32	84.36	0.31
2	243	30	8.87	5.77	4.58	12.56	87.37	0.08
3	266	30	9.76	5.26	4.58	15.27	84.72	0.01
4	289	30	7.86	5.14	4.18	13.91	86.08	0.00
5	312	30	9.82	5.53	4.38	12.70	86.37	0.93
6	220	218	7.17	26.25	4.18	15.70	84.3	0.00
7	243	218	12.05	6.01	4.79	14.29	85.71	0.00
8	266	218	9.20	6.06	6.53	14.11	85.89	0.00
9	289	218	9.37	5.23	4.38	16.32	83.68	0.00
10	312	218	9.79	6.21	4.58	12.70	87.30	0.00
11	220	406	9.19	5.88	4.58	13.67	86.33	0.00
12	243	406	9.31	5.67	4.79	13.83	86.17	0.00
13	266	406	7.96	5.65	5.25	12.61	87.39	0.00
14	289	406	7.58	4.91	4.18	15.41	84.59	0.00
15	312	406	10.82	6.32	4.75	13.27	86.73	0.00
16	220	594	6.55	4.38	3.99	19.86	80.14	0.00
17	243	594	9.68	5.37	4.38	15.58	84.32	0.10
18	266	594	8.21	5.44	5.02	14.28	85.72	0.00
19	289	594	8.19	4.88	4.38	18.62	81.38	0.00
20	312	594	9.47	5.34	4.38	15.08	84.92	0.00
21	220	782	6.58	4.38	3.99	17.04	82.96	0.00
22	243	782	7.67	4.92	4.58	15.84	84.16	0.00

Table A-4. Soil Particle Size Data and Sampling Coordinates from the FieldReclamation Site.

	X	у	Avera	age Values	(µm)		Clay	Silt
23	266	782	8.82	5.66	4.79	11.84	88.16	0.00
24	289	782	7.29	4.96	4.38	14.36	85.64	0.00
25	312	782	7.28	4.84	4.38	14.17	85.83	0.00
26	220	970	7.73	5.08	4.18	12.34	87.66	0.00
27	243	970	7.66	5.10	4.38	11.96	88.04	0.00
28	266	970	7.90	5.36	5.02	13.26	86.74	0.00
29	289	970	8.86	5.54	4.58	13.96	86.04	0.00
30	312	970	9.86	5.83	4.38	14.14	85.85	0.00
31	30	30	7.50	4.87	3.99	17.77	82.22	0.00
32	62.5	30	9.38	5.76	4.38	14.04	85.96	0.00
33	95	30	11.72	5.30	4.38	19.53	79.93	0.54
34	127.5	30	9.89	6.15	4.58	12.36	87.64	0.00
35	160	30	9.87	5.88	4.38	11.96	88.04	0.00
36	30	178	11.43	6.35	4.38	13.79	86.12	0.09
37	62.5	178	10.80	6.18	4.79	15.58	84.42	0.00
38	95	178	8.86	5.85	4.38	13.92	86.08	0.00
39	127.5	178	11.80	6.13	4.38	15.61	82.34	2.05
40	160	178	8.97	5.58	4.38	18.26	81.74	0.00
41	30	326	8.63	5.51	4.38	16.04	83.96	0.00
42	62.5	326	10.24	6.12	4.38	14.96	85.04	0.00
43	95	326	9.70	6.34	6.93	13.40	86.60	0.00
44	127.5	326	8.40	5.48	4.38	15.13	84.87	0.00
45	160	326	9.23	5.80	4.38	14.93	85.07	0.00
46	30	474	9.91	5.88	4.38	16.38	83.62	0.00
47	62.5	474	7.77	5.22	4.38	15.74	84.26	0.00
48	95	474	14.35	6.83	5.02	13.07	85.29	1.64

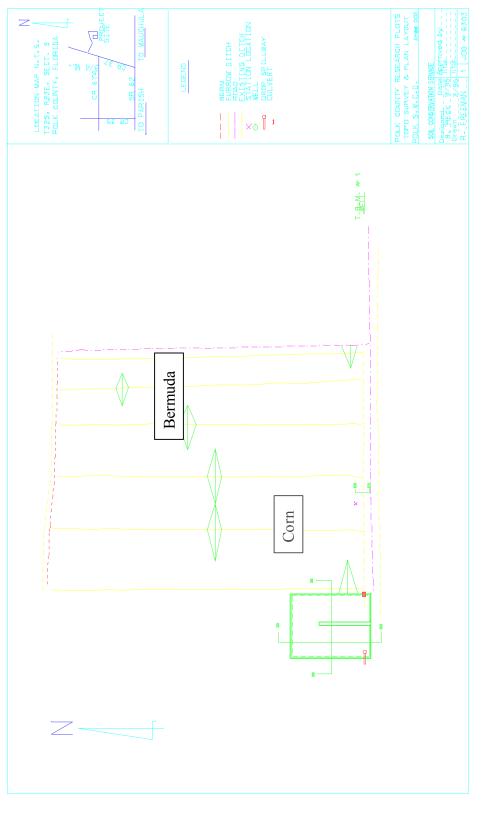
	X	у	Avera	age Values	(µm)		Clay	Silt
49	127.5	474	9.41	5.92	4.58	15.31	84.69	0.00
50	160	474	8.74	5.44	4.38	16.59	83.41	0.00
51	30	622	13.01	6.57	4.38	16.52	83.04	0.45
52	62.5	622	9.03	5.83	4.58	14.68	85.32	0.00
53	95	622	9.29	5.85	4.86	15.48	84.52	0.00
54	127.5	622	9.75	5.89	4.79	13.84	86.16	0.00
55	160	6.22	11.20	6.29	4.18	14.64	85.36	0.00
56	30	770	9.50	5.80	4.38	15.26	84.74	0.00
57	62.5	770	8.82	5.78	4.58	14.66	85.34	0.00
58	95	770	9.45	6.18	4.79	13.63	86.37	0.00
59	127.5	770	8.43	5.58	4.58	14.99	85.01	0.00
60	160	770	14.74	7.15	7.36	12.32	85.86	1.83
A	verage		9.30	5.99	4.61	14.74	85.13	0.134

	X	y (2)	Aver	age Values	(µm)		Clay	Silt
Sample	(ft)	(ft)	mean	median	mode	<2µm	2-64µm	>64µm
1	258	30	8.60	6.52	9.50	10.06	89.88	0.06
2	258	100	6.96	5.60	7.92	14.25	85.75	0.00
3	258	170	10.69	6.73	7.92	10.91	85.58	3.51
4	258	240	7.27	5.13	5.02	11.66	82.19	6.16
5	258	310	9.75	6.59	7.36	8.80	90.40	0.80
6	198	310	51.18	5.72	4.38	16.62	83.38	0.00
7	198	240	7.68	5.45	5.02	12.61	86.89	0.50
8	198	170	10.33	7.17	9.06	9.20	90.80	0.01
9	198	100	9.97	6.79	6.76	10.35	89.65	0.00
10	198	30	12.22	7.02	8.28	9.07	89.62	1.31
11	95	30	7.09	5.74	8.28	13.58	86.42	0.00
12	95	100	9.03	6.48	8.67	10.09	89.92	0.00
13	95	170	10.74	6.76	4.79	12.18	87.82	0.00
14	95	240	7.99	5.56	5.02	12.12	87.88	0.00
15	95	310	9.51	6.29	4.79	12.16	87.84	0.00
16	30	310	7.08	4.91	4.80	19.08	80.93	0.00
17	30	240	9.34	6.31	8.67	11.88	88.12	0.00
18	30	170	8.98	5.98	4.79	12.94	87.06	0.00
19	30	100	7.75	5.82	7.92	13.35	86.65	0.00
20	30	30	6.30	4.85	5.27	15.78	84.22	0.00
	Average		10.92	6.07	6.71	12.33	87.05	0.62

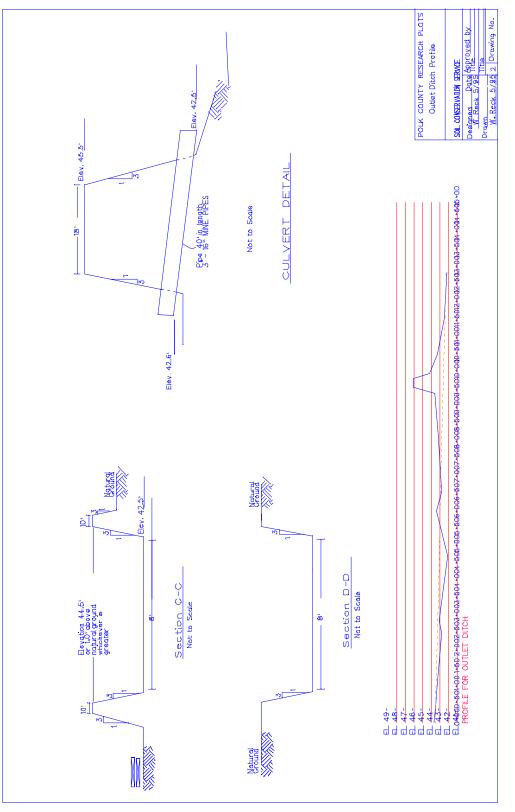
 Table A-5. Particle Size Data and Sampling Coordinates from the Overflow Pond Reclamation Site.

Appendix B

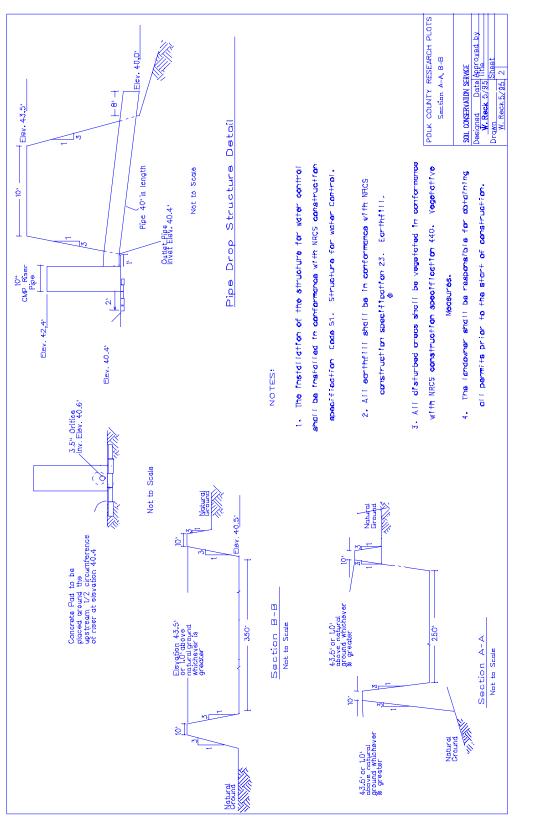
## LAYOUT AND CONSTRUCTION DETAILS FOR MACROBED EXPERIMENT













Appendix C

## CHEMICAL TREATMENT OF SUSPENDED SOLIDS IN MINED-LANDS RUNOFF WATERS

## LABORATORY DATA

FIPR Project, 1997													
Total P (perchloric digestion) and Ca fr	oric diges	tion) a	nd Ca froi	om same digestion	igestion		_				Final		
10 mL of shaken sample to a final solution after digestion of 100 mL	en sample	to a fi	nal solutio	in after di	gestion of	100 mL.							
				Starting									
				Turbidity	Initial	Dosing	mdd	after	Hd	Settling	Turbidity		
Setno Reported	Labno	ID#	Sample#	(NTU)	Hq	Compound	Fe/Al	Ηd	adjusted	ime (min	UTN	G	Ъ
e													
6200 18-Jun-97	97 130376		1		7.44	FeCl3	3.4	6.43	7.00	8	232.00	127	24
6200 18-Jun-97	97 130377		2		7.44	FeC13	6.7	6.00	8.02	30	255.00	116	22
6200 18-Jun-97	97 130378	Э	3		7.44	FeC13	13.4	3.80	7.20	30	29.20	124	3
6200 18-Jun-97	97 130379		4	242	7.44	FeC13	20.2	3.51	7.00	30	12.50	100	
6200 18-Jun-97	37 130380	S	IJ		7.44	FeC13	26.9	3.24	7.60	99	8.40	113	1
6200 18-Jun-97	<u> </u>		9		7.44	FeC13	33.6	3.25	7.00	30	15.60	122	1
6200 18-Jun-97	97 130382	7	2		7.44	FeC13	40.3	2.19	7.00	30	8.10	129	1
6200 18-Jun-97	97 130383	8	8	141	7.44	Fecta	134	462	212	œ	377,00	117	22 77 very high end turbidity
6200 18-Jun-97	130384	6	6		7.26	FeC13	3.4	5.41	7.35	30	474.00	137	
	37 130385	10	10		7.49	FeCI3	6.7	4.30	7.50	8	472.00	143	36
	37 130386	11	11		7.45	FeC13	13.4	3.77	7.20	8	186.70	110	
6200 18-Jun-97		12			7.55	FeCl3	20.2	3.44	7.25	8	45.20	83	
6200 18-Jun-97	97 130388	13			7.38	FeC13	26.9	3.28	7.30	30	18.10	109	2
6200 18-Jun-97					7.73	FeCl3	33.6	3.23	7.05	8	27.40	118	
6200 18-Jun-97	37 130390	15			7.81	FeCl3	40.3	3.18	7.65	8	13.80	143	
6200 18-Jun-97		16		267	7.67	FeC13	26.9	3.33	7.16	8	58.20	108	
6200 18-Jun-97	97 130392	17			7.40	FeC13	3.4	4.38	8.00	30	216.00	96	13
6200 18-Jun-97	7 130393			105	8.00	FeCl3	6.7	3.78	6.98	30	233.00	105	14
6200 18-Jun-97	97 130394				7.78	FeC13	13.4	3.52	7.00	30	40.00	88	2
6200 18-Jun-97	97 130395		20	105	7.82	FeC13	20.2	3.35	7.00	30	9.70	104	1
6200 18-Jun-97	97 130396		21		7.70	FeC13	26.9	3.35	7.25	30	7.24	55	
6200 18-Jun-97	7 130397				7.83	FeC13	33.6	3.34	8.00	30	5.31	69	0
6200 18-Jun-97	97 130398				7.83	FeC13	40.3	3.25	7.30	30	7.60	11	0
6200 18-Jun-97	97 130399	24			7.90	FeC13	26.9	3.43	8.75	30	13.74	53	0
6200 18-Jun-97	7 130400				7.26	FeCI3	3.4	5.41	7.35	450	155.80	29	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
6200 18-Jun-97	7 130401			267	7.49	FeCl3	6:∕J	4.30	7.50	450	52.60	ຊ	
6200 18-Jun-97	7 130402				7.45	FeC13	13.4	3.77	7.20	450	2.28	ŝ	0
6200 18-Jun-97	7 130403	28			7.55	FeC13	20.2	3.44	7.25	450	0.86	39	
6200 18-Jun-97	7 130404	29			7.38	FeCI3	26.9	3.28	7.30	450	0.70	53	0
6200 18-Jun-97	130405				7.73	FeCl3	33.6	3.23	7.05	450	0.64	88	0
6200 18-Jun-97	130406		31		7.81	FeC13	40.3	3.18	7.65	450	0.77	80	0
6200 18-Jun-97	130407	32	32		7.67	FeC13	26.9	3.33	7.16	450	0.97	8	0
	130408	33	33		7.40	FeC13	3.4	4.38	8.00	450	428.00	92	36
6200 18-Jun-97	130409		34		8.00	FeC13	6.7	3.78	6.98	450	57.10	22	4
6200 18-Jun-97	130410	35			7.78	FeCl3	13.4	3.52	7.00	450	8.87	24	1
6200 18-Jun-97	130411		36		7.82	FeC13	20.2	3.35	7.00	450	2.80	37	0
6200 18-Jun-97	7 130412		37		7.70	FeC13	26.9	3.35	7.25	450	2.25	49	0
6200 18-Jun-97	7 130413	38	38	105	7.83	FeCl3	33.6	3.34	8.00	450	1.92	60	0
6200 18-Jun-97	7 130414		39	105	7.83	FeCl3	40.3	3.25	7.30	450	1.79	75	1
6200 18-Jun-97	7 130415	40	40	105	06.2	For 13	090	2 12	8 75 8	150	721	46	U
į					~~~	1721	20.7		0.10	₽	5	40	-

	1//7 hadar														
Total P	, (perchlor	ic digest	ion) a	Total P (perchloric digestion) and Ca from		same digestion						Final			
10 mL	of shaken	sample t	to a fii	10 mL of shaken sample to a final solution	n after di	after digestion of 100 mL	100 mL.								
					Starting										
				Ę	<b>Furbidity</b>	Initial	Dosing	mqq	after	ΡH	Settling	Turbidity			
Setno	Reported	Labno	ID#	Sample#	(NTU)	Ηd	Compound	Fe/Al	Hq	adjusted		DTN	Ca	Ч	
Adcode	0														
6200	18-Jun-97	130416	41	41	361	7.70	e2(SO4)	3.4	6.71	 7.33	- 95 -	414.00	235	68	
6200	18-Jun-97	130417	42	42	361	7.86	e2(SO4)	6.8	6.32	ZZ	8	467.00	246	93	
6200	18-Jun-97	130418	43	43	361	7.90	e2(SO4)	13.6	5.04	7.49	85	215.00	ភ	Ħ	
6200	18-Jun-97	130419	44	4	361	7.92	e2(SO4)	20.4	4.20	7.44	80	48.00	20	3	
6200	18-Jun-97	130420	45	45	361	7.93	e2(SO4)	27.3	3.65	7.55	75	26.30	R	2	
6200	18-Jun-97	130421	46	46	361	7.86	e2(SO4)	34.1	3.35	7.70	8	15.70	94	+4	
6200	18-Jun-97	130422	47	47	361	7.98	e2(SO4)	40.9	3.24	7.56	33	16.30	120	7	
6200	18-Jun-97	130423	48	48	361	7.98	e2(SO4)	27.3	4.20	8.23	80	39.50	ន្ល	9	
6200	18-Jun-97	130424	49	49	539	7.85	e2(SO4)	3.4	6.65	7.80	100	547.00	135	50	
6200	18-Jun-97	130425	50	50	543	7.70	e2(SO4)	6.8	5.80	7.20	100	536.00	155	57	
6200	18-Jun-97	130426	51	51	520	7.60	e2(SO4)	13.6	3.81	7.50	60	47.80	54	10	
6200	18-Jun-97	130427	52	52	535	7.60	e2(SO4)	20.4	3.35	7.75	85	20.40	92	2	
6200	18-Jun-97	130428	53	53	545	7.65	e2(SO4)	27.3	3.31	7.90	80	14.30	127	1	
6200	18-Jun-97	130429	2	52	533	7.80	e2(SO4)	34.1	3.10	8.50	75	6.44	159	3	
6200	18-Jun-97	130430	55	55	534	7.80	e2(SO4)	40.9	3.05	7.80	70	12.10	162	1	
6200	18-Jun-97	130431	5	56	535	7.80	e2(SO4)	27.3	3.40	8.50	65	21.50	86	2	
6200	18-Jun-97	130432	57	57	361	7.70	e2(SO4)	3.4	6.71	7.33	1350	499.00	158	<b>4</b>	
6200	18-Jun-97	130433	58	58	361	7.86	e2(SO4)	6.8	6.32	7.71	1350	152.40	82	13	
6200	18-Jun-97	130434	56	59	361	7.90	e2(SO4)	13.6	5.04	7.49	1350	13.14	62	, ,	
6200	18-Jun-97	130435	99	99	361	7.92	e2(SO4)	20.4	4.20	7.44	1350	1.40	143	0	
6200	18-Jun-97	130436	61	61	361	7.93	e2(SO4)	27.3	3.65	7.55	1350	1.16	120	0	
6200	18-Jun-97	130437	62	62	361	7.86	e2(SO4)	<b>34.1</b>	3.35	7.70	1350	1.21	147	0	
6200	18-Jun-97	130438	63	63	361	7.98	e2(SO4)	40.9	3.24	7.56	1350	1.06	172	0	
6200	18-Jun-97	130439	64	64	361	7.98	e2(SO4)	27.3	4.20	8.23	1350	1.60	<b>9</b> 4	0	
6200	18-Jun-97	130440	3	65	539	7.85	e2(SO4)	3.4	6.65	7.80	1450	406.00	172	43	
6200	18-Jun-97	130441	66	66	543	7.70	e2(SO4)	6.8	5.80	7.20	1450	133.60	103	12	
6200	18-Jun-97	130442	67	67	520	7.60	e2(SO4)	13.6	3.81	7.50	1450	2.97	63	0	
6200	18-Jun-97	130443	68	68	535	7.60	e2(SO4)	20.4	3.35	7.75	1450	1.12	89	0	
6200	18-Jun-97	130444	69	69	545	7.65	e2(SO4)	27.3	3.31	7.90	1450	1.21	115	0	
6200	18-Jun-97	130445	70	70	533	7.80	e2(SO4)	34.1	3.10	8.50	1450	1.20	86	0	
6200	18-Jun-97	130446	7	7	534	7.80	e2(SO4)	40.9	3.05	7 80	1450	1 30	177	c	
0007						and the second s						1	1/2	>	

	FIPR	FIPR Project, 1997	26													
f shaken sample to a final solution after digestion of 100 mL         A	Total	P (perchlo	ric diges	tion) a	und Ca fro		igestion						Final			
Reported         Lathing         Darthing         Initial         Dosing         ppm         after         pH         Settling         Initiality           Reported         Lahoo         [D#         Sample#         (NTU)         PH         Compound         Fe/Al         PH         Settling         Initiality           Reported         Lahoo         [D#         Sample#         (NTU)         PH         Compound         Fe/Al         PH         Settling         Initiality           Reported         Lahoo         [D#         Sample#         (NTU)         PH         Compound         Fe/Al         PH         Settling         Initiality         Ca           Repurery         130413         75         Alum         3.8         4.52         7.65         30         137         7.8           Repurery         130451         77         211         7.40         Alum         7.5         4.00         7.33         30         1.71         102           Repurery         130451         77         211         7.40         Alum         7.5         4.00         7.33         30         1.71         102           Repurery         130451         76         Alum         7.5 <td>10 ml</td> <td>L of shaken</td> <td>ı sample</td> <td>to a fi</td> <td>nal solutic</td> <td></td> <td>igestion of</td> <td>100 mL.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	10 ml	L of shaken	ı sample	to a fi	nal solutic		igestion of	100 mL.								
Image         Turblidik         Initial         Desing         ppm         after         pH         Settling         Turblidik           lepuney         labuo         ID#         Sample#         (NTU)         pH         compound         Fe/Al         pH         Settling         Turblidik           lepuney         13044         73         73         201         7.35         Alum         3.8         4.52         7.65         30         19.59         118         74           lepuney         130440         77         77         202         810         Alum         7.5         419         9.00         30         18.66         117         102           lepuney         130450         77         77         202         810         Alum         7.5         4.19         9.00         107         102           lepuney         130450         77         202         810         Alum         371         3.85         7.20         30         117         102           lepuney         130450         81         353         7.50         Alum         372         3.95         133         232           lepuney         130450         81         35						Starting										
Reported         Labor         ID#         Sample#         (NTU)         pH         Compound         Fe/AI         pH         adjusted         inft         NTU         Ca           18/mey         130445         73         73         201         7.55         Alum         3.8         4.57         7.65         30         19.59         160         113           18/mey         130451         77         77         7.55         Alum         7.51         4.198         9.00         30         18.8         7.4           18/mey         130451         77         77         221         7.40         Alum         37.5         3.89         7.25         30         1.171         102           18/mey         130451         77         721         7.40         Alum         37.7         3.89         7.28         30         1.171         102           18/mey         130451         77         221         Alum         37.7         388         7.43         7.4           18/mey         130455         81         81         57.30         3.18         97         7.4           18/mey         130456         81         8.00         Alum						Turbidity		Dosing	mdd	after	Hq	Settling	Turbidity			
Islumy	Setno	Reported	Labno	1D#		(NTU)		Compound	Fe/AI	Hq	adjusted	ime (min		Ca	Р	
Islums         130445         73         201         7.35         Alum         3.8         4.52         7.65         3.0         19.59         160           Islums         130446         73         73         201         7.35         Alum         7.5         4.19         9.06         30         18.60         113           Islums         130445         75         77         202         810         Alum         7.5         4.19         9.06         30         18.60         113           Islums         130451         76         7.6         Alum         27.5         30         1.81         74           Islums         130451         76         7.7         202         810         Alum         37.1         4.08         7.20         30         1.71         102           Islums         130451         77         221         810         Alum         37.1         3.99         7.25         30         1.71         102           Islums         130451         77         221         Alum         37.1         4.00         7.20         30         1.71         102           Islums         130455         81         Alum	Adcoc	de														
16Juney         130445         73         70         735         Alum         3.8         4.52         7.65         30         19.59         160 $18$ Juney         130445         74         74         190         8.05         Alum         7.5         4.19         9.00         30         18.60         113 $18$ Juney         13045         7         7         202         8.10         Alum         5.51         4.08         7.20         30         15.53         108 $18$ Juney         13045         7         76         203         7.50         30         1.81         74 $18$ Juney         13045         78         70         Alum         22.6         Alum         3.73         3.99         7.20         30         1.71         102 $18$ Juney         13045         81         8.10         Alum         3.71         3.99         7.23         30         1.71         102 $18$ Juney         13045         81         8.10         Alum         3.71         3.99         7.28         30         1.71         102 $18$ Juney         13045         81         8.10         A																
Iblumy         130448         73         201         7.35         Alum         3.8         4.52         7.65         30         19.59         100           Iblumy         130441         74         74         198         8.05         Alum         7.5         4.19         9.00         30         15.55         108           Iblumy         130451         7         77         77         201         8.10         Alum         2.51         3.99         7.25         30         1.71         102           Iblumy         130451         76         78         2.24         8.00         Alum         3.7         3.85         7.20         30         1.71         102           Iblumy         130451         78         2.24         8.00         Alum         3.7         3.85         7.20         3.0         1.71         102           Iblumy         130451         81         81         53         7.40         Alum         3.7         3.90         3.01         1.71         102           Iblumy         130451         81         81         53         7.40         Alum         3.7         3.90         3.18         9.7           I												and the second second				
IbJum-y7         130449         74         74         198         8.05         Alum         7.5         4.19         9.00         30         18.60         113           1bJum-y7         130450         75         75         202         8.10         Alum         22.6         399         7.25         30         18.1         74           1bJum-y7         130451         7         7         203         7.65         Alum         30.7         399         7.20         30         1.71         102           1bJum-y7         130451         79         78         224         8.00         Alum         37.7         385         7.20         30         1.71         102           1bJum-y7         130451         79         79         221         8.10         Alum         37.7         389         7.20         30         1.71         102           1bJum-y7         130451         81         81         533         7.25         Alum         37.7         389         7.20         30         1.71         102           1bJum-y7         130451         81         81         500         7.29         30         1.32         20         1.32	6200		_				7.35	Alum	3.8	4.52	7.65	30	19.59	160	<b></b> 1	
1b) m.yr         130450         75         77         202         8.10         Alum         15.1         4.08         7.20         30         6.55         108           1bJm.yr         130451         76         77         221         8.10         Alum         226         3.99         7.25         30         1.71         102           1bJm.yr         130451         79         77         221         8.10         Alum         37         3.85         7.20         30         1.71         102           1bJm.yr         130451         79         77         3.85         7.20         30         1.71         102           1bJm.yr         130451         81         53         7.25         Alum         3.61         4.00         7.38         30         1.13         229           1bJm.yr         130451         82         81         54         7.00         Alum         377         3.85         7.40         30         1.23         1.23           1bJm.yr         130461         86         83         7.40         7.40         30         1.23         1.29           1bJm.yr         130461         86         551         7.50	6200						8.05	Alum	ŝ	4,19	9:00	30	18.60	113	<b></b>	-
18 Jun-y         13045         7         7         7.5         A lunn         22.6         3.90         7.25         3.0         1.81         7.4           18 Jun-y         13045         77         77         721         7.40         Alunn         37.1         3.80         7.20         1.01         1.02           18 Jun-y         13045         77         7         221         7.40         Alunn         37.7         3.85         7.20         30         1.71         102           18 Jun-y         13045         81         81         523         7.25         Alunn         37.7         3.85         7.20         30         1.171         102           18 Jun-y         13045         82         83         5.45         7.90         Alunn         37.5         4.40         10.00         30         8.77         126           18 Jun-y         13045         82         545         7.50         Alunn         37.7         4.40         10.00         30         8.77         126         126           18 Jun-y         13046         83         553         7.57         Alunn         37.7         4.40         10.00         30         12.78	6200						8.10	Alum	15.1	4.08	7.20	30	6.55	108	÷	
IbJun-yr         13045         77         77         721         7.40         Alum         301         3.90         7.30         30         1.71         102           IbJun-yr         130453         78         78         724         8.00         Alum         377         385         7.20         30         1.07         126           IbJun-yr         130458         81         780         Alum         377         385         7.20         30         1.107         126           IbJun-yr         130458         81         81         55.3         7.50         Alum         37.7         399         7.24         80         107         126           IbJun-yr         130457         82         82         7.50         Alum         7.5         4.40         10.00         30         8.25         123         7.7           IbJun-yr         130450         82         84         7.60         Alum         37.7         30         30         6.73         173         172         172           IbJun-yr         130450         85         553         7.70         30         12.56         175         172         141         760         30	6200			76			7.65	Alum	22.6	3.99	7.25	30	1.81	74	0	
18 Jun-97         130453         78         78         224         8.00         Alum         37.7         3.85         7.20         30         1.07         126           18 Jun-97         130454         79         79         79         221         8.10         Alum         45.2         3.99         7.28         30         11.13         229           18 Jun-97         130456         81         8.30         Alum         301         4.00         7.38         30         11.3         229           18 Jun-97         130456         81         81         5.53         7.26         Alum         7.5         4.40         7.00         30         8.23         90         137           18 Jun-97         130460         85         85         553         7.75         Alum         2.75         4.40         7.60         30         12.64         132           18 Jun-97         130460         85         85         553         7.75         Alum         37.7         3.97         7.60         30         13.60         137           18 Jun-97         130460         86         86         551         7.95         Alum         3.97         7.60         <	6200						7.40	Alum	30.1	3.90	7.30	30	1.7	102	0	
Is Jun-97         130454         79         721         8.10         Ahun         45.2         3.99         7.28         30         1.13         229           Is Jun-97         130455         81         80         368         8.30         Ahun         30.1         4.00         7.38         30         1.13         229           Is Jun-97         130456         81         81         553         7.25         Ahun         3.8         5.00         7.90         30         32.00         137         97           Is Jun-97         130456         81         83         545         7.90         Alun         7.5         4.40         10.00         30         8.25         132         97           Is Jun-97         130460         85         83         545         7.90         Alun         30.1         3.97         7.40         30         12.58         90         175           Is Jun-97         130461         86         551         7.95         Alun         30.1         4.05         7.60         30         6.24         152         179         175           Is Jun-97         130461         86         551         7.95         Alun <td< td=""><td>6200</td><td></td><td></td><td></td><td></td><td></td><td>8.00</td><td>Ahum</td><td>37.7</td><td>3.85</td><td>7.20</td><td>30</td><td>1.07</td><td>126</td><td>0</td><td></td></td<>	6200						8.00	Ahum	37.7	3.85	7.20	30	1.07	126	0	
18 Jun-97         130455         80         80         8.30         Alum         30.1         4.00         7.38         30         31.8         97           18 Jun-97         130455         81         81         553         7.25         Alum         3.8         5.00         7.90         30         392.00         137         97           18 Jun-97         130457         82         82         7.60         Alum         7.5         4.40         10.00         30         8.25         132         90         137           18 Jun-97         130458         83         545         7.90         Alum         25.6         4.00         7.30         30         8.25         132         132           18 Jun-97         130460         85         85         553         7.75         Alum         30.1         3.97         7.60         30         13.60         137         216         17.9           18 Jun-97         130461         86         551         7.95         Alum         37.7         3.92         7.75         30         15.6         17.9         179         179         179         179         179         179         179         175         176<	6200						8.10	Ahum	45.2	3.99	7.28	30	1.13	229	0	
18/un-97         130456         81         81         553         7.25         Alum         3.8         5.00         7.90         30         392.00         137           18/un-97         130457         82         548         7.60         Alum         7.5         4.40         10.00         30         8.25         132         90           18/un-97         130457         82         548         7.60         Alum         7.5         4.40         10.00         30         8.25         132         90           18/un-97         130460         85         85         553         7.75         Alum         22.6         4.00         7.30         30         8.25         132         179         130           18/un-97         130461         86         551         7.95         Alum         30.1         3.97         7.60         30         13.60         156         176           18/un-97         130461         86         551         7.95         Alum         30.1         4.00         7.50         30         13.60         156         176           18/un-97         130461         91         91         3.75         3.86         7.70         3	6200						8.30	Alum	30.1	4.00	7.38	30	3.18	66	0	
Is Jun-97         130457         82         548         7.60         Alum         7.5         4.40         10.00         30         8.25         132         132           Is Jun-97         130457         83         545         7.90         Alum         15.1         4.05         7.40         30         8.25         132         90           Is Jun-97         130463         84         84         549         7.65         Alum         22.6         4.00         7.30         30         8.09         126         90         90         126         157         159         126         150         126         126         175         150	6200						7.25	Alum	3.8	5.00	7.90	30	392.00	137	33	
18 Jun-97         130458         83         545         7.90         Alum         15.1         4.05         7.40         30         12.38         90           18 Jun-97         130458         84         549         7.65         Alum         22.6         4.00         7.30         30         8.09         126           18 Jun-97         130460         85         553         7.75         Alum         30.1         3.97         7.60         30         6.24         152           18 Jun-97         130461         86         551         7.95         Alum         37.7         3.92         7.35         30         6.24         152           18 Jun-97         130461         86         86         551         7.95         Alum         37.7         3.92         7.36         37.7         216         77.9         216         175           18 Jun-97         130465         90         90         325         7.45         Alum         7.55         3.86         5.77         216         73.6         73.6         73.6         73.6         73.6         73.6         73.6         73.6         73.6         73.6         73.6         73.6         73.6         73.6	6200						7.60	Alum	7.5	4.40	10.00	30	8.25	132	1	
Is Jun-97         130459         84         549         7.65         Alum         22.6         4.00         7.30         30         8.09         126         126           18 Jun-97         130460         85         553         7.75         Alum         30.1         3.97         7.60         30         6.24         152         153         179         152         152         152         153         150         152         152         152         153         153         150         156         157         156         156         156         156         156         156         156         156         157         156         157         156         156         156         156         156         156         156         156         156         156         157	6200						7.90	Alum	15.1	4.05	7.40	30	12.38	8	1	
Is Jun-97         130460         85         553         7.75         Alum         30.1 $3.97$ 7.60         30         6.24         152           18 Jun-97         130461         86         551         7.95         Alum $37.7$ $3.92$ $7.35$ $30$ $6.73$ $179$ 179           18 Jun-97         130461         86         551         7.95         Alum $37.7$ $3.92$ $7.35$ $30$ $6.73$ $179$ $216$ 18 Jun-97         130462         87         86 $8.10$ Alum $30.1$ $4.00$ $7.50$ $30$ $5.87$ $216$	6200						7.65	Alum	22.6	4.00	7.30	30	8.09	126	1	
18.Jun-97         130461         86         551         7.95         Alum $37.7$ $3.92$ $7.35$ $30$ $6.73$ $179$ $179$ 18.Jun-97         130461         87         562         7.95         Alum $45.2$ $3.86$ $7.70$ $30$ $5.87$ $216$ $216$ 18.Jun-97         130461         89         88         560         8.10         Alum $30.1$ $4.00$ $7.50$ $30$ $13.60$ $156$ $156$ 18.Jun-97         13046         91         91 $332$ $7.45$ Alum $7.5$ $4.25$ $7.50$ $900$ $23.60$ $7.3$ 18.Jun-97         13046         91         91 $335$ $7.80$ Alum $7.5$ $4.25$ $7.40$ $900$ $23.60$ $7.3$ 18.Jun-97         13046         91 $335$ $7.80$ Alum $20.5$ $4.25$ $7.40$ $900$ $0.76$ $104$ 18.Jun-97         13046         91 $3.355$ $7.90$ <td>6200</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>7.75</td> <td>Alum</td> <td>30.1</td> <td>3.97</td> <td>7.60</td> <td>30</td> <td>6.24</td> <td>152</td> <td>1</td> <td></td>	6200						7.75	Alum	30.1	3.97	7.60	30	6.24	152	1	
18.Jun-97         130462         87         562         7.95         Alum         45.2         3.86         7.70         30         5.87         216           18.Jun-97         130463         88         560         8.10         Alum         30.1         4.00 $7.50$ 30         13.60         156           18.Jun-97         130464         89         329         7.45         Alum         3.8         4.44 $7.60$ 900         23.60         73           18.Jun-97         13046         91         91         332         7.45         Alum         7.5         4.25 $7.50$ 900         23.60         73           18.Jun-97         130467         92         328 $7.80$ Alum         21.6         4.00 $7.40$ 900         0.76         131           18.Jun-97         13046         91         335 $7.80$ Alum         30.1 $3.98$ $7.24$ 900         0.76         131           18.Jun-97         130470         92         325 $7.90$ Alum         37.7         3.89 $7.24$ 900         0.76         131	6200			86			7.95	Alum	37.7	3.92	7.35	30	6.73	179	1	
18.Jun-97         130463         88         560         8.10         Alum         30.1         4.00 $7.50$ 30         13.60         156	6200			87			7.95	Alum	45.2	3.86	7.70	30	5.87	216	8	
18/um-97         1304.4         89         329         7.45         Alum         3.8         4.44         7.60         900         23.60         73           18/um-97         1304.65         90         90         332         7.65         Alum         7.5         4.25         7.50         900         23.60         73           18/um-97         1304.65         91         91         332         7.65         Alum         7.5         4.25         7.50         900         2.62         89           18/um-97         1304.67         92         92         328         7.80         Alum         22.16         4.00         7.45         900         0.76         131           18/um-97         1304.69         94         94         369         8.00         Alum         37.7         3.89         7.24         900         0.76         131           18/um-97         1304.70         95         95         8.00         Alum         37.7         3.89         7.24         900         0.45         172           18/um-97         1304.70         95         95         8.00         Alum         37.7         3.89         7.24         900         0.46	6200						8.10	Alum	30.1	4.00	7.50	8	13.60	156	2	
18/1m-97         130465         90         90         332         7.65         Alum         7.5         4.25 $7.50$ 900         2.62         89           18/1m-97         130466         91         91         335         7.80         Alum         15.1         4.15         7.40         900         2.62         89           18/1m-97         130467         92         92         328         7.80         Alum         15.1         4.15         7.40         900         0.84         104           18/1m-97         130469         94         93         355         7.90         Alum         30.1         3.98         7.24         900         0.58         148           18/1m-97         130470         95         95         8.00         Alum         37.7         3.89         7.20         900         0.45         172           18/1m-97         130470         95         95         360         7.95         Alum         37.7         3.89         7.20         900         0.45         172           18/1m-97         130470         96         96         8.00         Alum         37.7         3.89         7.20         900 <td< td=""><td>6200</td><td></td><td></td><td></td><td></td><td></td><td>7.45</td><td>Ahum</td><td>3.8</td><td>4.44</td><td>7.60</td><td>006</td><td>23.60</td><td>2</td><td>N</td><td></td></td<>	6200						7.45	Ahum	3.8	4.44	7.60	006	23.60	2	N	
18 Jun-97         130466         91         91         335         7,80         Alum         15.1         4.15         7.40         900         0.84         104           18 Jun-97         130467         92         92         328         7.80         Alum         22.6         4.00         7.45         900         0.76         131           18 Jun-97         130469         94         94         369         8.00         Alum         30.1         3.98         7.24         900         0.76         131           18 Jun-97         130469         94         94         369         8.00         Alum         37.7         3.89         7.20         900         0.45         172           18 Jun-97         130470         95         95         8.00         Alum         45.2         3.89         7.20         900         0.45         172           18 Jun-97         130471         96         96         8.00         Alum         30.1         3.99         7.40         900         0.45         172           18 Jun-97         130471         96         96         8.00         Alum         30.1         3.99         7.40         900         0.45	6200						7.65	Ahum	7.5	4.25	7,50	006	2.62	89	<b>1-4</b>	
18/um-97         130467         92         92         328         7.80         Alum         22.6         4.00         7.45         900         0.76         131           18/um-97         130468         93         93         355         7.90         Alum         30.1         3.98         7.24         900         0.76         134           18/um-97         130469         94         94         369         8.00         Alum         37.7         3.89         7.24         900         0.58         148           18/um-97         130470         95         95         8.00         Alum         37.7         3.89         7.20         900         0.45         172           18/um-97         130470         95         96         7.95         Alum         30.1         3.99         7.40         900         0.94         193           18/um-97         130471         96         96         8.00         Alum         30.1         3.99         7.40         900         0.94         193	6200			91	61		7.80	Alum	15.1	4.15	7.40	006	0.84	104	0	
18/un-97         130468         93         93         355         7.90         Alum         30.1         3.98         7.24         900         0.58         148           18/un-97         130469         94         94         369         8.00         Alum         37.7         3.89         7.20         900         0.45         172           18/un-97         130470         95         95         360         7.95         Alum         45.2         3.85         7.31         900         0.94         193           18/un-97         130471         96         96         8.00         Alum         30.1         3.99         7.40         900         0.94         193           18/un-97         130471         96         96         8.00         Alum         30.1         3.99         7.40         900         1.46         124	6200						7.80	Ahum	22.6	4.00	7.45	006	0.76	131	0	
18/Jun-97         130469         94         94         369         8.00         Alum         37.7         3.89         7.20         900         0.45         172           18/Jun-97         130470         95         95         360         7.95         Alum         45.2         3.85         7.31         900         0.94         193           18/Jun-97         130471         96         96         8.00         Alum         30.1         3.99         7.40         900         1.46         124	6200						7.90	Alum	30.1	3.98	7.24	006	0.58	148	0	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	6200						8.00	Alum	37.7	3.89	7.20	906	0.45	172	0	
18.Jun-97 130471 96 96 366 8.00 Alum 30.1 3.99 7.40 900 1.46	6200						7.95	Ahum	45.2	3.85	7.31	006	0.94	193	0	
	6200			96			8.00	Alum	30.1	3.99	7.40	006	1.46	124	•	

LIFR Froject, 1997	(nlert' 12)											_		
Total P	(perchloi	ic digesti	Total P (perchloric digestion) and Ca from	rom same d	same digestion						Final			
10 mL (	of shaken	sample t	10 mL of shaken sample to a final solution	tion after di	after digestion of 100 mL.	100 mL.								
				Starting										
				Turbidity	Initial	Dosing	bpm	after	PH S	Settling Turbidity	urbidity			
Setno Reported	Reported	Labno	ID# Sample#	(NTU) #	Hq	Compound	Fe/Al	Hq	adjusted ir	ime (min	NTU	Ca ]	P	
Adcode														
				Turbidity	Turbidity Mean Median	Median								
				(NTU)	(microns	(NTU) (microns (microns	Ca	4	P and Ca cc	orrelations	P and Ca correlations with NTUxMean, NTU x Median	Mean, NTI	U x Median	
6200	18-Jun-97	130472	97 101	_ 360	1.138	0.627	138	37	aı	nd NTU w	and NTU with a 0.97 Rsq. (No intercept)	q. (No int	ercept)	
6200	18-Jun-97	130473	98 10		0.864	0.752	190	56						
6200	18-Jun-97	130474	99 10	103 211	1.556	1.750	98	16	TP= (0.197x	<b>NTUXMe</b>	TP= (0.197xNTUxMean) - (0.170xNTUxMedian)	NTUxMed	lian) 0.97 Rsq	
6200	18-Jun-97	18-Jun-97 130475	100 10	104 158	1.256	0.896	80	12						
6200	18-Jun-97	130476	101 10	105 521	5.031	3.697	528	193	TCa= (0.252	2×NTU) -	(0.481×NTU	(Median)	TCa= (0.252xNTU) - (0.481xNTUxMedian) + (0.495xNTUxMean)	0.97 Rsq
6200	18-Jun-97	18-Jun-97 130477	102 10		2.945	2.585	190	56						
6200	18-Jun-97	130478	103 10	107 362	2.525	2.314	114	26	TP = (0.404)	xTCa) - 2(	$TP = (0.404 \times TCa) - 20.348  0.999 \text{ Rsq}$	Ssq		
6200	18-Jun-97	130479	104 10	<u>8</u> 290	1.647	1.587	111	26						
6200	18-Jun-97 130480		105 10	109 102	0.846	0.566	Ч	6	* computed with SAS (9/18/97)	with SAS	(9/18/97)			
6200	18-Jun-97	130481	106 STD150P	LT LT			58	148						
6200	18-Jun-97	130482	18-Iun-97 130482 107 STD150P	DP			54	136						

C-5

Mined Lands Project - Sedimentation Removal

Chemical Calculation Sheet

287.7526 Fe2(SO4)3	162.206 FeCl3	101.9612 AI2O3			(1.85 g/L solubility)
Fe	S	0	ច	AI	74.09 Ca(OH)2
55.847 Fe	32.064	15.9994	35.453	26.9815	74.09

0.38816 FE : Fe2(SO4)3 0.344297 FE : FeCl3 0.52925 AL : AI2O3

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1.488 specif gravity (g/co) 44.3 % FeCl3 15.252 % Fe (II) 152.523 ppm Fe

FERRIC SULFATE 1.467 specifc gravity (g/cc) 25.2 % Fe2(SO4)3 9.8 % Fe (III) 98,000 ppm Fe

12/18/96

FERRIC CHLORIDE

	1000 ml	mL to 1000 ml	0.5	-	7	რ	4	5	9	4
	eigh aut into om AL		2000	1000	500	333	250	200	167	250
	235,008 W 7536 pi	ppm Fe Dilution	3.8	7.5	15.1	22.6	30.1	37.7	45.2	30.1
: ppm second.	o 1000 mi	mL to 1000 ml	0.5	-	2	ო	4	5	9	4
calculated: the 1,000	igh out inf m Fe		2000	1000	500	333	250	200	167	250
1 ppm addition of Fe, the following is calculated: mical. Make a 10,000 ppm first, then the 1,000 p	65,564 weigh ou 6720 ppm Fe	ppm Fe Di	3.4	6.7	13.4	20.2	26.9	33.6 200	40.3	26.9
ppm addition of F nical. Make a 10,0	nto 1000 ml	mL to 1000 ml	0.5	-	2	ო	4	S	9	4
to make 1 each chem	eigh out int om Fe		2000	1000	500	333	250	200	167	250
nl addition olution for	102.041 weigh ou 6817 ppm Fe	ppm Fe Dilution	3.4	6.8	13.6	20.4	27.3	34.1	40.9	27.3
For a 1 ml to 1000 ml addition to make 1 ppm addition of Fe, the following is calculated: Need a 1000 ppm solution for each chemical. Make a 10,000 ppm first, then the 1,000 ppm second. $\frac{7}{7}$	10,000 ppm = 102.041 weigh out in 6817 ppm Fe			2	ς	4	5	9	7	80

111 0000 111	mL to 1000 ml	0.5	-	2	ო	4	5	9	4
eigh out into om Fe	ilution ml	2000	1000	500	333	250	200	167	250
65,564 weightouth 6720 ppm Fe	ppm Fe D	3.4	6.7	13.4	20.2	26.9	33.6	40.3	26.9
<ul> <li>102.041 weigh out into 1000 ml</li> <li>6817 ppm Fe</li> </ul>	mL to 1000 ml	0.5	-	2	ო	4	5	9	4
weigh out in oom Fe	Dilution n	2000	1000	500	333	250	200	167	250
102.041 6817	ppm Fe	3.4	6.8	13.6	20.4	27.3	34.1	40.9	27.3
= udd			2	ო	4	5	9	7	ω

D.L. Anderson